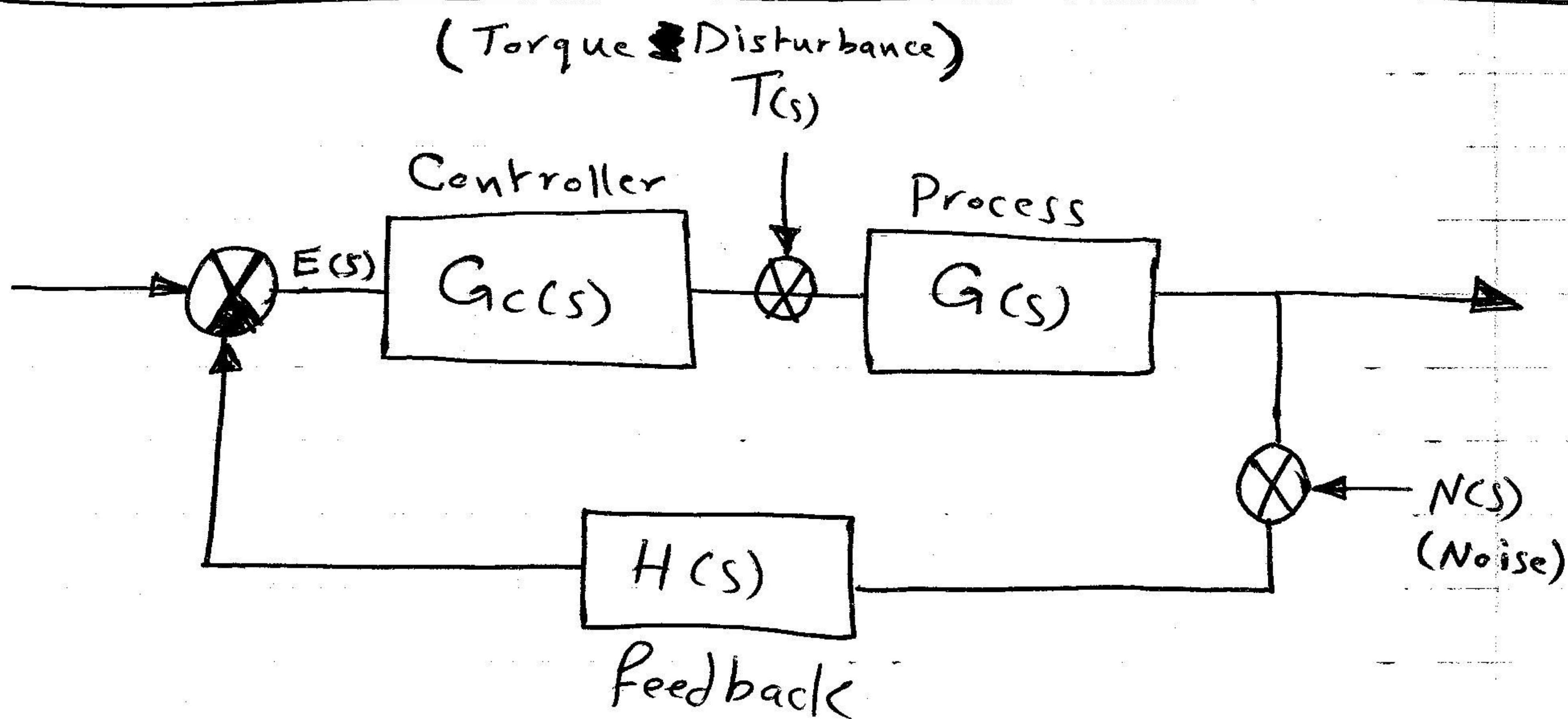


The Steady State Error of a feedback Control System



$$E(s) = R(s) - C(s) H(s) \implies H(s) = 1$$

$$\therefore E(s) = R(s) - C(s)$$

$$\otimes E(s) = R(s) - C(s)$$

$$H(s) = 1$$

$$= R(s) \left[1 - \frac{C(s) H(s)}{R(s)} \right]$$

$$= R(s) \left[1 - \frac{G_c(s) G(s) H(s)}{1 + G_c(s) G(s) H(s)} \right]$$

$$= R(s) \left[\frac{1 + G_c(s) G(s) H(s) - G_c(s) G(s) H(s)}{1 + G_c(s) G(s) H(s)} \right]$$

$$= \frac{1}{1 + G_c(s) G(s) H(s)} * R(s)$$

1

⊛ If $R(s) = \frac{A}{s}$ (Step Input).

$$E(s) = \frac{A/s}{1 + G(s)G(s)H(s)}$$

$$e_{ss} = \lim_{t \rightarrow \infty} e(t) = \lim_{s \rightarrow 0} s E(s)$$

$$= \lim_{s \rightarrow 0} s * \frac{A/s}{1 + G(s)G(s)H(s)}$$

$$= \frac{A}{1 + G(s)G(s)H(s)}$$

⊛ The Loop transfer function is given by :-

$$G(s)G(s)H(s) = \frac{k \prod_{i=1}^M (s - z_i)}{s^N \prod_{k=1}^Q (s - p_k)}$$

~~z_i : أصف - قطب~~ z_i : أصف - قطب p_k : أصف - مقام

Ex

$$\frac{2}{3s^2} \times \frac{3(s+1)}{s^2+1} \times \frac{(s-2)}{s^3+s+1} = \frac{6(s+1)(s-2)}{3s^2(s^2+1)(s^3+s+1)}$$

⊛ k : حاصل قسمة ثابت التردد في البسط على ثابت التردد في المقام

$$\text{total Gain} \leftarrow \textcircled{2} = \frac{6}{3} = k \text{ في المثال السابق}$$

⊕ The No of integration is often indicated by Labeling a system with a type Number that is equal to N.

⊕ The steady State tracking error for a step input of magnitude "A" is given by :-

$$e_{ss} = \frac{A}{1+K_p} \quad \text{for type Zero.}$$

⊕ K_p : Positioning Constant

⊕ If the system has more than one integration, then

$$e_{ss} = \text{Zero}$$

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$$E(s) = \frac{R(s)}{1+G_c(s)G(s)H(s)}$$

2

⊕ If $R(s) = \text{Ramp input} = \frac{A}{s^2}$

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s^2}{1+G_c(s)G(s)H(s)} = \lim_{s \rightarrow 0} \frac{A}{sG_c(s)G(s)H(s)}$$

⊗ If the system is type Zero $\Rightarrow N=0$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s \times k} = \frac{A}{0} = \infty$$

⊛ If the system is type 1 $\Rightarrow N=1$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s * \frac{K_v}{s}} = \boxed{A/K_v}$$

K_v : Velocity Constant

$$G_c(s) G(s) H(s) = \frac{K \prod_{i=1}^M (s - z_i)}{s^N \prod_{k=1}^Q (s - p_k)}$$

⊛ If the system is type 2 $\Rightarrow N=2$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} \frac{A}{s * \frac{k}{s^2}} = \frac{A}{\frac{k}{s}} = \frac{A}{\infty} = \boxed{\text{Zero}}$$

In the case of Ramp Input, we need two

Integrators to eliminate the error.

⊛ [3] If $R(t) = \frac{At^2}{2} \Rightarrow R(s) = \frac{A}{s^3}$

“Acceleration Input”

$$E(s) = \frac{R(s)}{1 + G_c(s) G(s) H(s)} = \frac{A/s^3}{1 + G_c(s) G(s) H(s)}$$

$$e_{ss} = \lim_{s \rightarrow 0} s^1 \frac{A/s^3}{1 + G_c(s) G(s) H(s)} = \lim_{s \rightarrow 0} \frac{A}{s^2 G_c(s) G(s) H(s)}$$

Q $N=0 \Rightarrow e_{ss} = \infty$

$N=1 \Rightarrow e_{ss} = \infty$

$N=2 \Rightarrow e_{ss} = \frac{A}{K_a}$

$N=0 \Rightarrow G_c G_H(s) = K_1$

$N=1 \Rightarrow G_c G_H(s) = \frac{K_2}{s}$

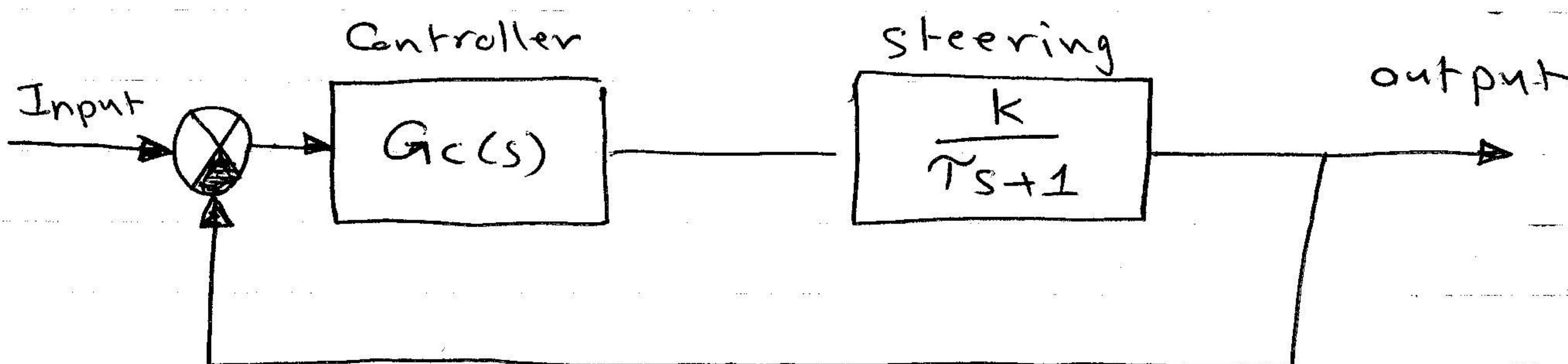
$N=2 \Rightarrow G_c G_H(s) = \frac{K_3}{s^2}$

K_a = Acceleration Constant

Type \ Input	Unit step $r(t) = A$ $R(s) = A/s$	Ramp Input $r(t) = At$ $R(s) = A/s^2$	Acceleration Input $r(t) = At^2/2$ $R(s) = A/s^3$
$N=0$	$\frac{A}{1+K_p}$	∞	∞
$N=1$	Zero	$\frac{A}{K_v}$	∞
$N=2$	Zero	Zero	$\frac{A}{K_a}$

Ex: Mobile Robot may be designed as an assisting device or servant for disabled person.

- The steering Control system for a such robot can be represented by



here we used PI- Controller
"given in the question"

Case 1 : If $R(s) = \text{Unit Step Input} = \frac{A}{s}$

$$\text{If } G_c(s) = \frac{k_1 s + k_2}{s} = \boxed{\frac{k_1 + \frac{k_2}{s}}{s}}$$

↑ ↑
P I Controller

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s}{1 + G_c G H(s)} = \frac{A}{1 + G_c G H(s)}$$

$$G_c G H(s) = \frac{k_1 s + k_2}{s} * \frac{k}{\tau s + 1} = \frac{k_2 * k}{s}$$

$$\therefore e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s}{1 + G_c G H(s)} = \frac{A}{1 + G_c G H(s)} = \frac{A}{1 + \frac{k_2 k}{s}} = \boxed{\text{Zero}}$$

Case 2 : If $R(s) = \text{Ramp Input} = \frac{A}{s^2}$

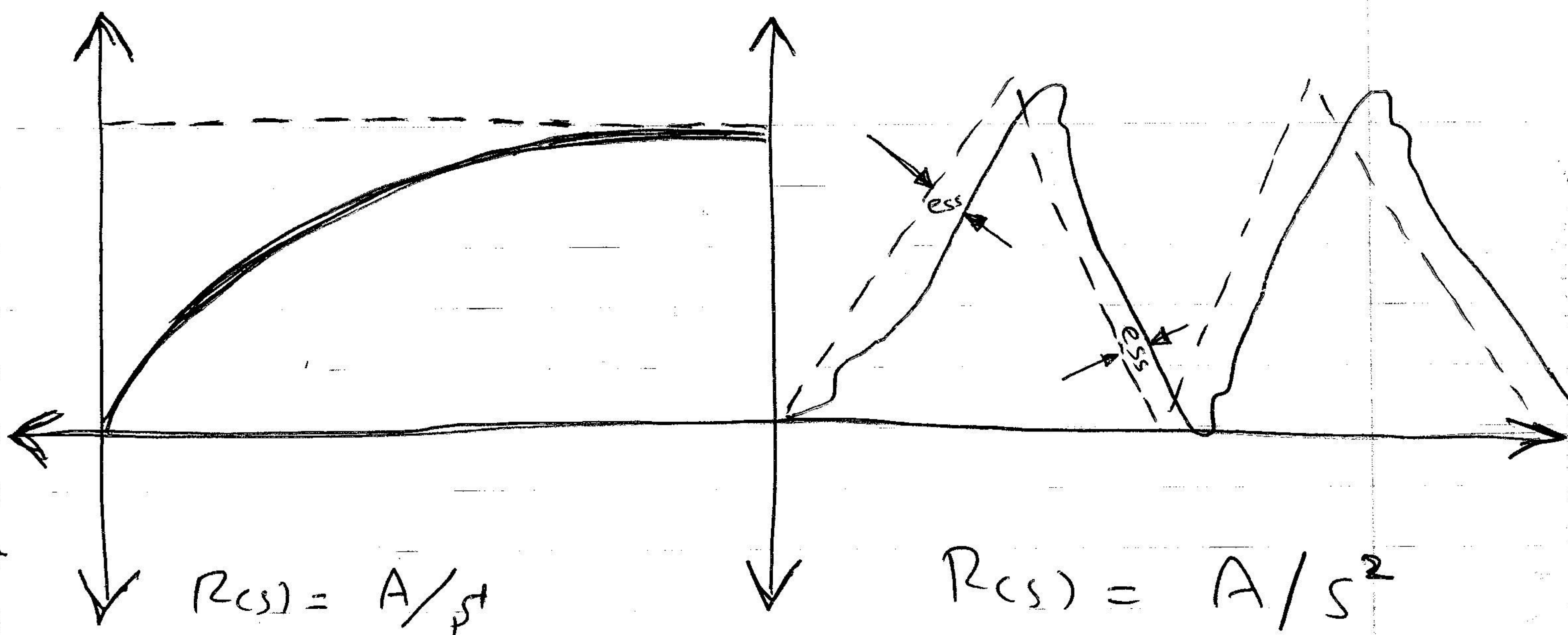
With PI Controller

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{A/s^2}{1 + G_c G H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{A}{s G_c G H(s)}$$

$$= \lim_{s \rightarrow 0} \frac{A}{s * \frac{k_2 k}{s}} = \boxed{\frac{A}{k_2 k}}$$

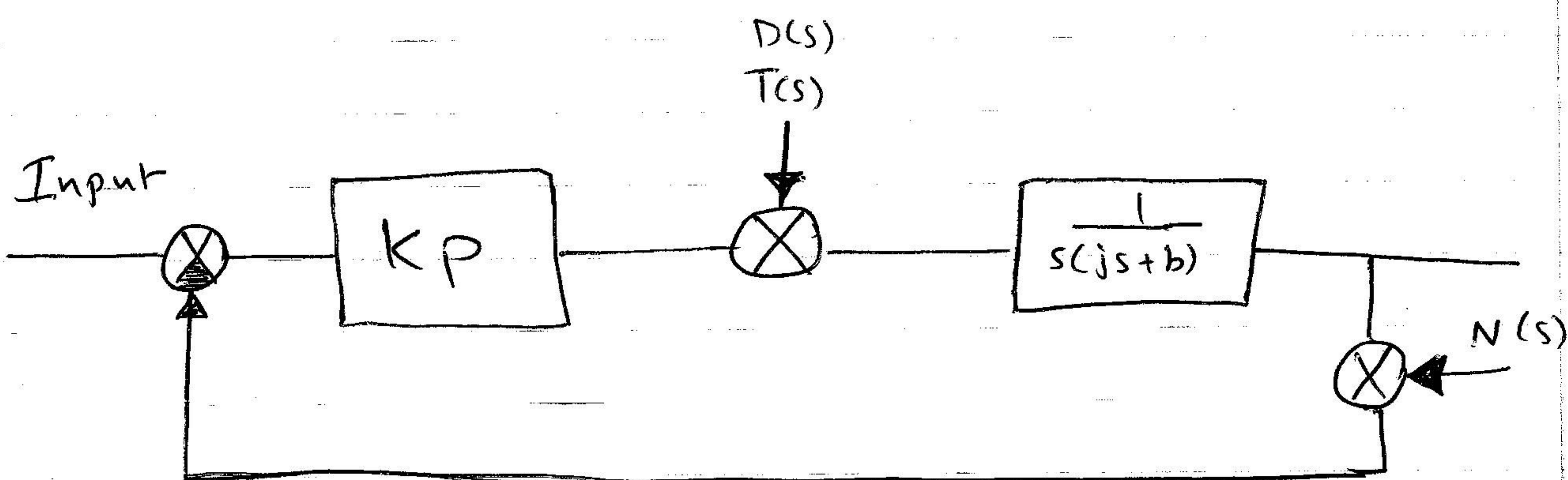
$k_2 k$: Velocity Constant



In the case of Ramp Input, we need two Integrators to Eliminate the error.

11/26 SCW

① Response to torque (Proportional Controller)

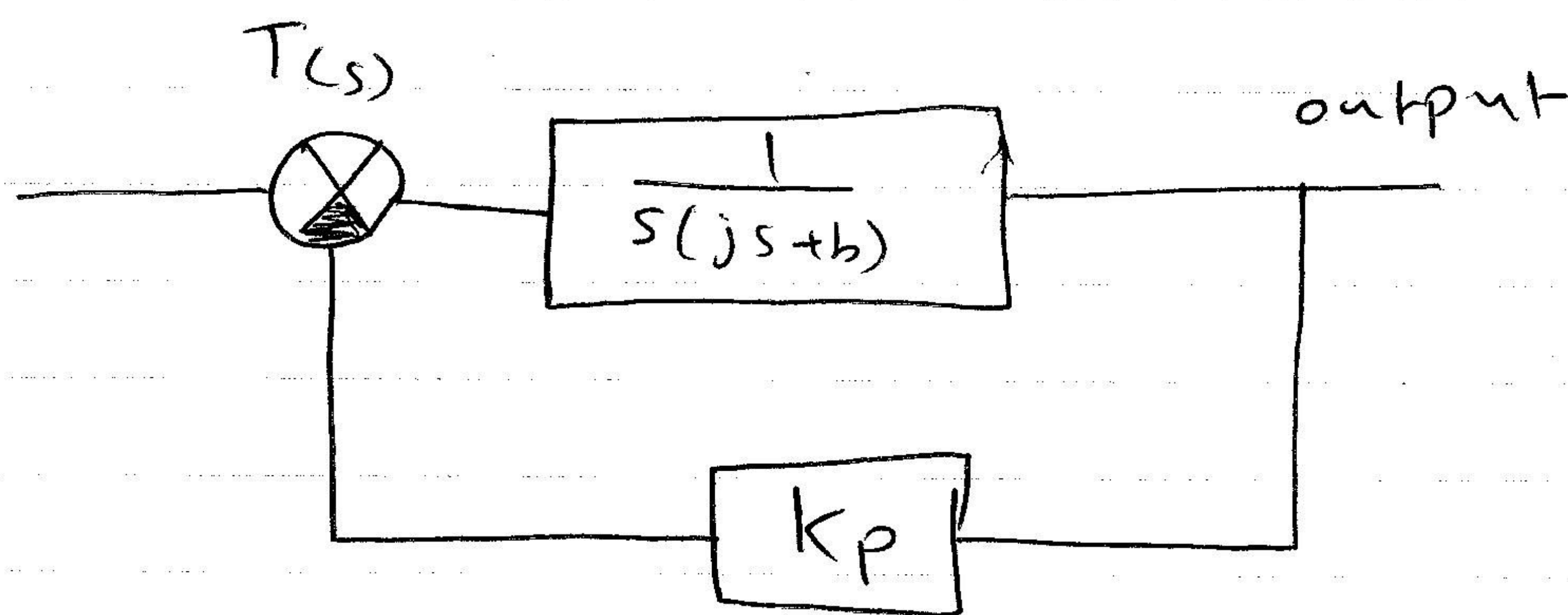


- ① Set Input to Zero
- ② Set $N(s) = \text{Zero}$
- ③ Rearrange the control diagram

Input = 0

$$N(s) = 0$$

⇒ Now Rearrange the control diagram as follows:-



$$\otimes E(s) = \text{Input} - \text{Output}$$

$$= \text{Zero} - \text{Output}$$

$$= \text{Zero} - C(s) = \boxed{-C(s)}$$

$$\otimes \frac{C(s)}{D(s)} = \frac{\frac{1}{s(js+b)}}{\frac{1}{s(js+b)} * kp + 1} = \frac{1}{s(js+b) + kp}$$
$$= \boxed{\frac{1}{js^2 + bs + kp}}$$

$$\otimes \therefore \frac{E(s)}{D(s)} = \frac{-C(s)}{D(s)} = \boxed{\frac{-1}{js^2 + bs + kp}}$$

$$\therefore E(s) = \boxed{\frac{-Ds}{js^2 + bs + kp}}$$

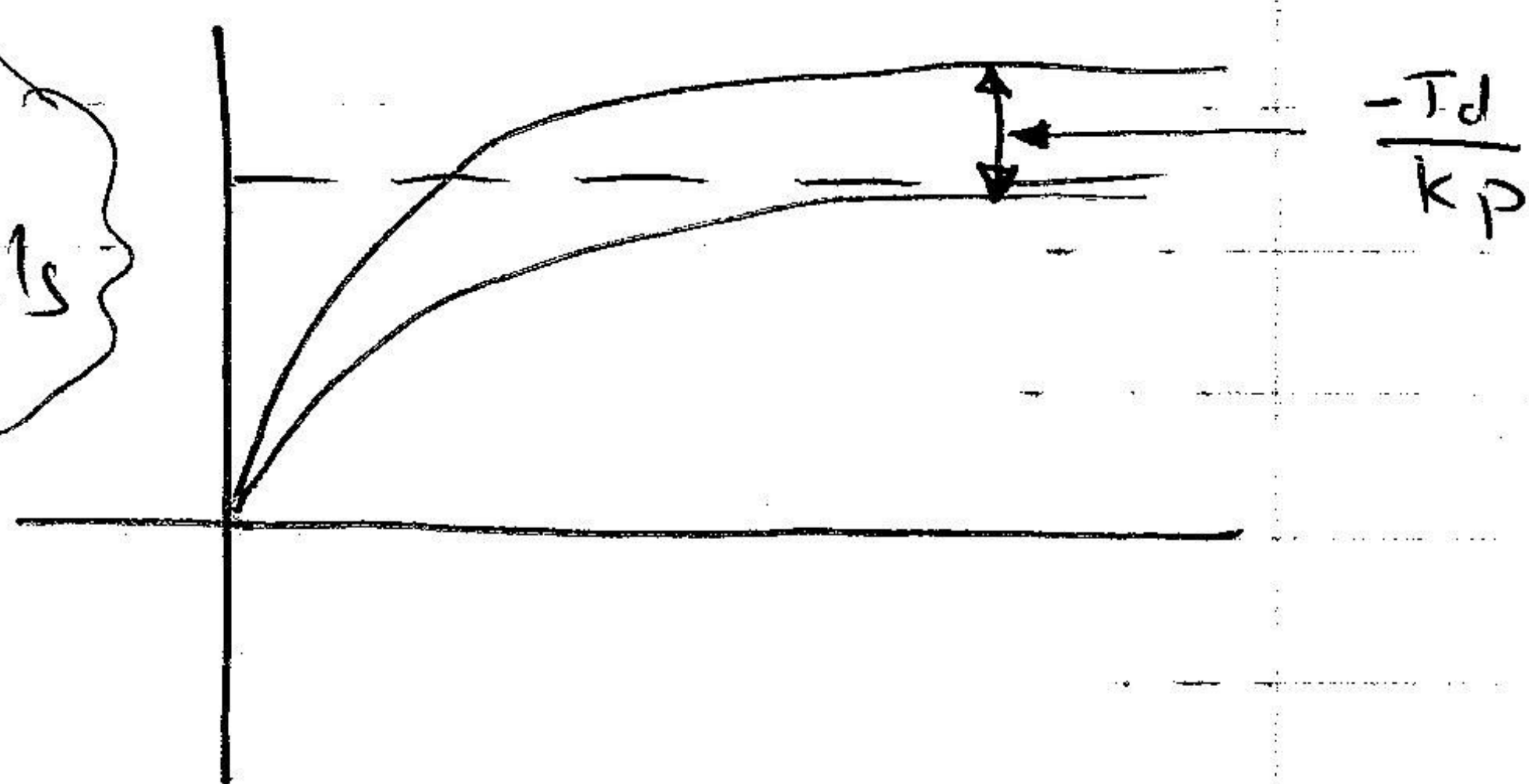
$D(s)$ is a unit Step disturbance $\Rightarrow D(s) = \frac{T_d}{s}$

$$e_{ss} = \lim_{s \rightarrow 0} s \frac{-\frac{T_d}{s}}{js^2 + bs + kp}$$

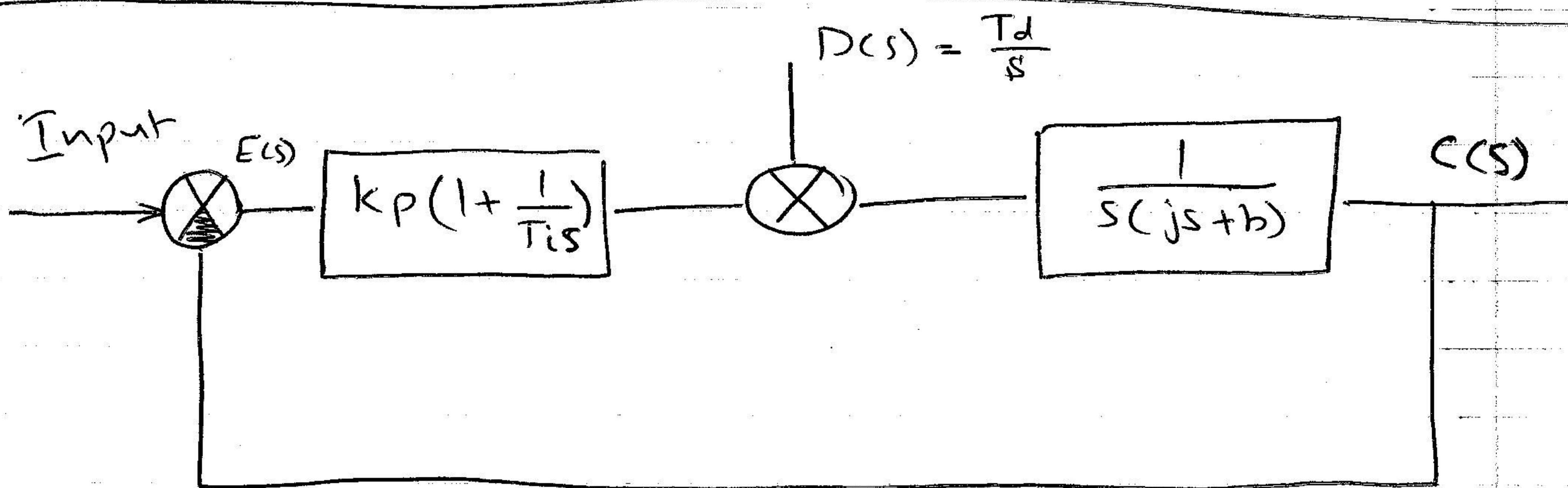
$$= \lim_{s \rightarrow 0} \frac{-T_d}{js^2 + bs + kp} = \frac{-T_d}{j(0)^2 + b(0) + kp}$$

$$= \boxed{\frac{-T_d}{kp}}$$

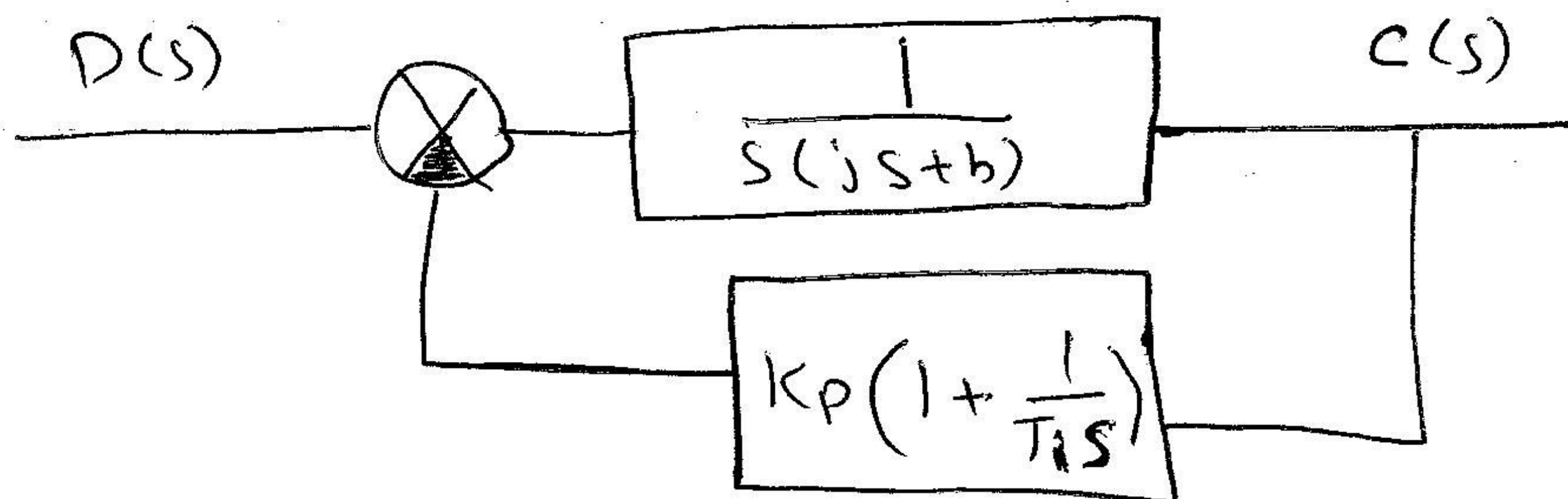
∴ The P-controller Cannot eliminate the error and equals it to zero, but it can decrease the error.



② Response to torque (PI-Controller)



\Rightarrow Rearrange the Control diagram (input = zero)



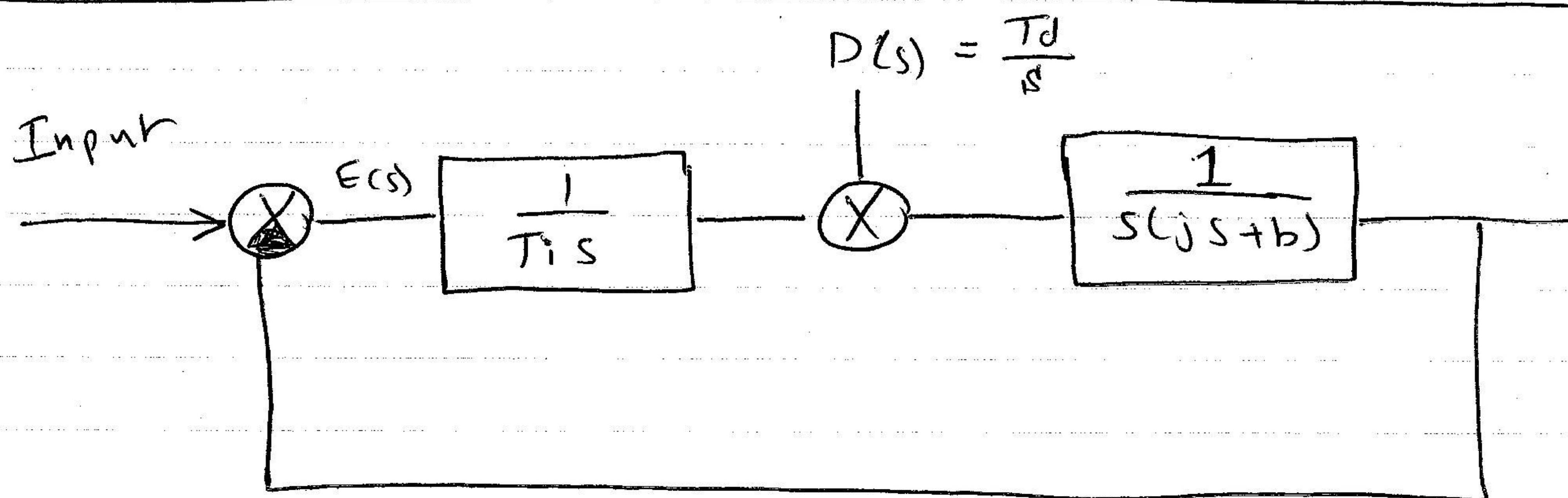
$$\lim_{s \rightarrow 0} \frac{E(s)}{D(s)} = \frac{-s}{Js^3 + bs^2 + kps + \frac{kp}{Ti}}$$

$$\Rightarrow e_{ss} = \lim_{s \rightarrow 0} s \frac{-s \frac{T_d}{s}}{Js^3 + bs^2 + kps + \frac{kp}{Ti}}$$

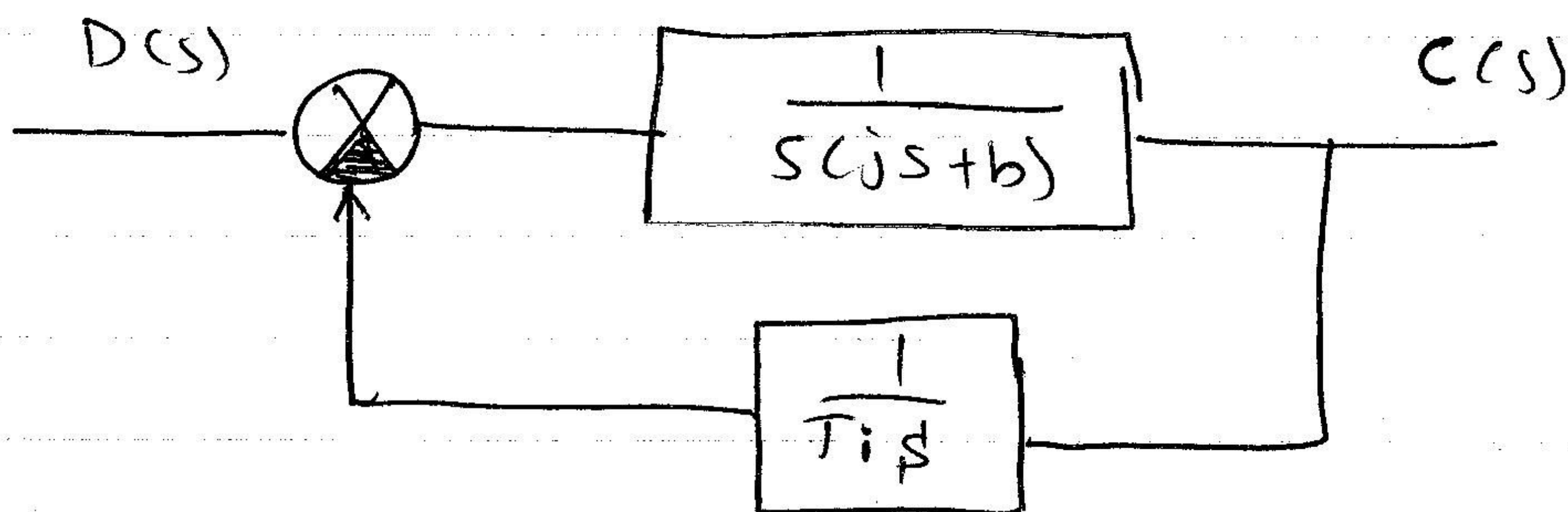
$$= \boxed{\text{Zero}}$$

∴ Using the PI-Controller eliminate the error

③ Response to torque (I-Controller only)



⇒ Rearrange the control diagram (Input = 0)



$$\begin{aligned}
 \frac{C(s)}{D(s)} &= \frac{1}{s(j s + b)} = \frac{1}{\frac{1}{s(j s + b)} * \frac{1}{T_i s} + 1} = \frac{1}{\frac{1}{T_i s} + s(j s + b)} \\
 &= \frac{T_i s}{1 + T_i s^2(j s + b)} \\
 &= \frac{T_i s}{1 + T_i j s^3 + T_i b s^2} = \frac{C(s)}{D(s)}
 \end{aligned}$$

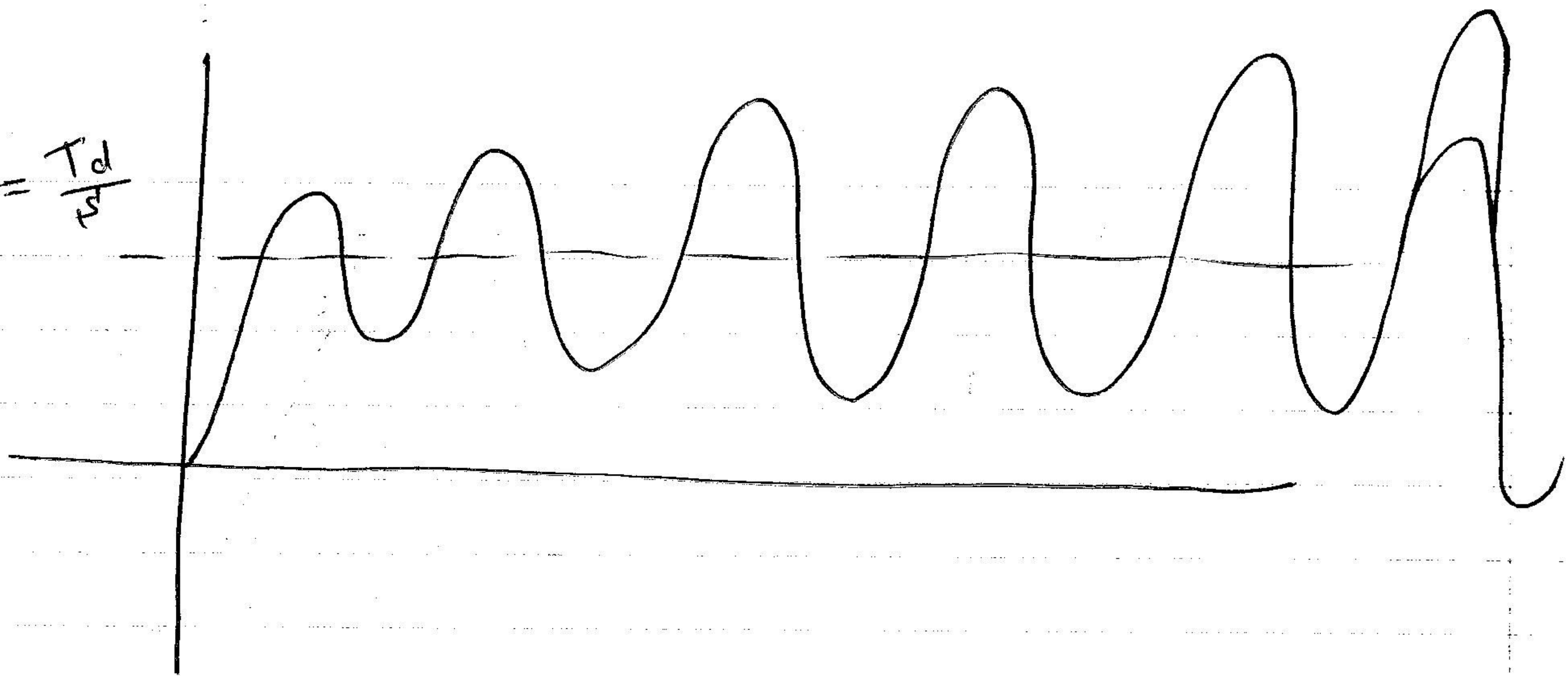
$$\begin{aligned}
 \infty e_{ss} &= \lim_{s \rightarrow 0} s \frac{T_i s * \frac{T_d}{s}}{1 + T_i j s^3 + T_i b s^2} \\
 &= \boxed{\text{Zero}}
 \end{aligned}$$

$$\frac{C(s)}{D(s)} = \frac{T_i s}{T_i j s^3 + T_i b s^2 + 1}$$

s^3	$T_i j$	0
s^2	$T_i b$	1
s	$\left(\frac{-j}{b}\right)$	0
1	1	

The system is unstable !!

$$D(s) = \frac{T_d}{s}$$



⊗ :- We must Use PI-Controller to eliminate the error and to maintain the stability of the system.

⊗ Using I-Controller only eliminate the errors but the system is "Unstable".

Performance Indices

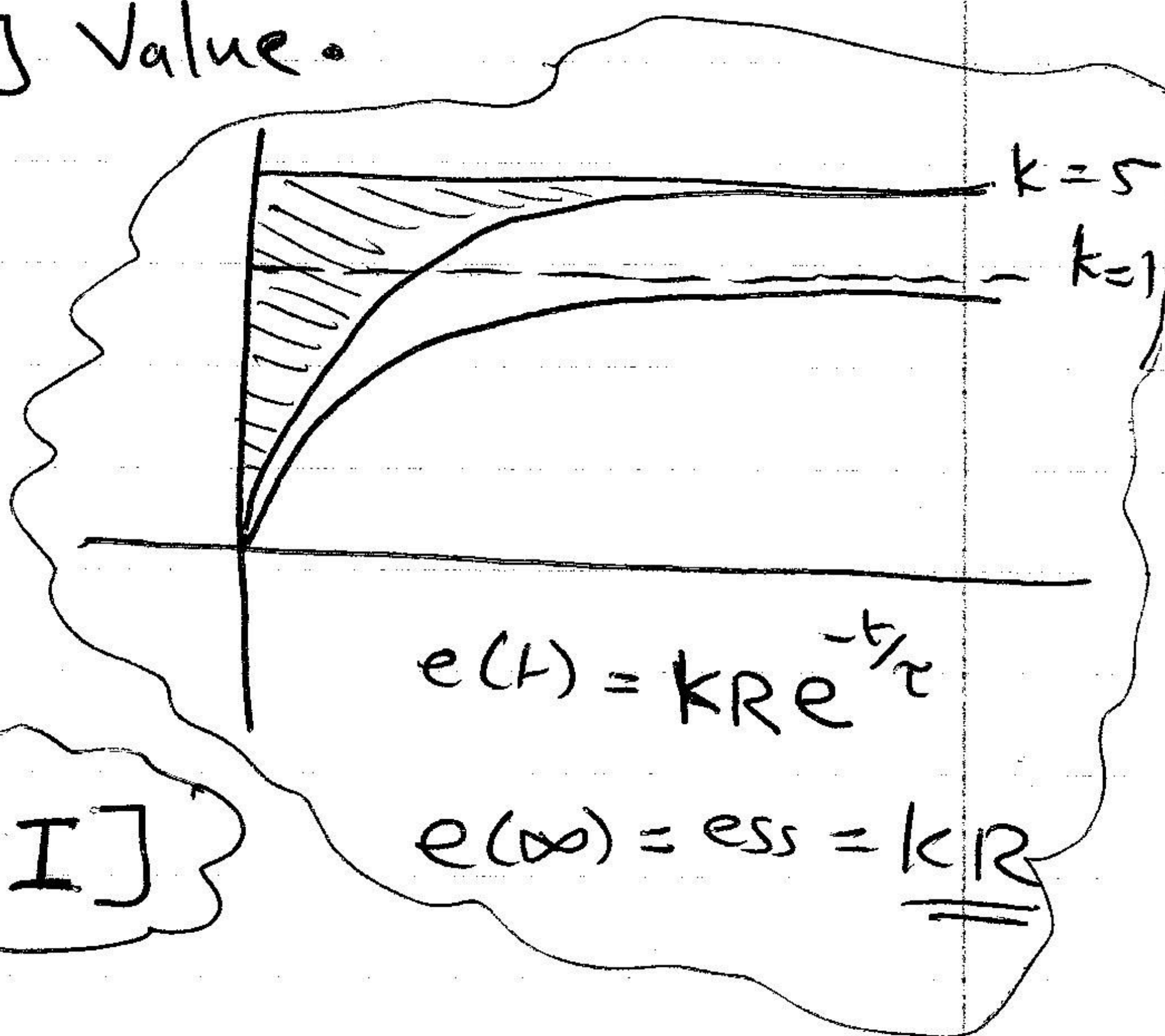
[Dorf 5.7]

⊗ A performance index J is a quantitative measure of the performance of a system, and is chosen so that emphasis is given to the important system specifications

⊗ a system is ~~is~~ considered an optimum control system when the system parameters are adjusted so that the index reaches its extremum [minimum] value.

⊗ a performance index must be a number that is always positive

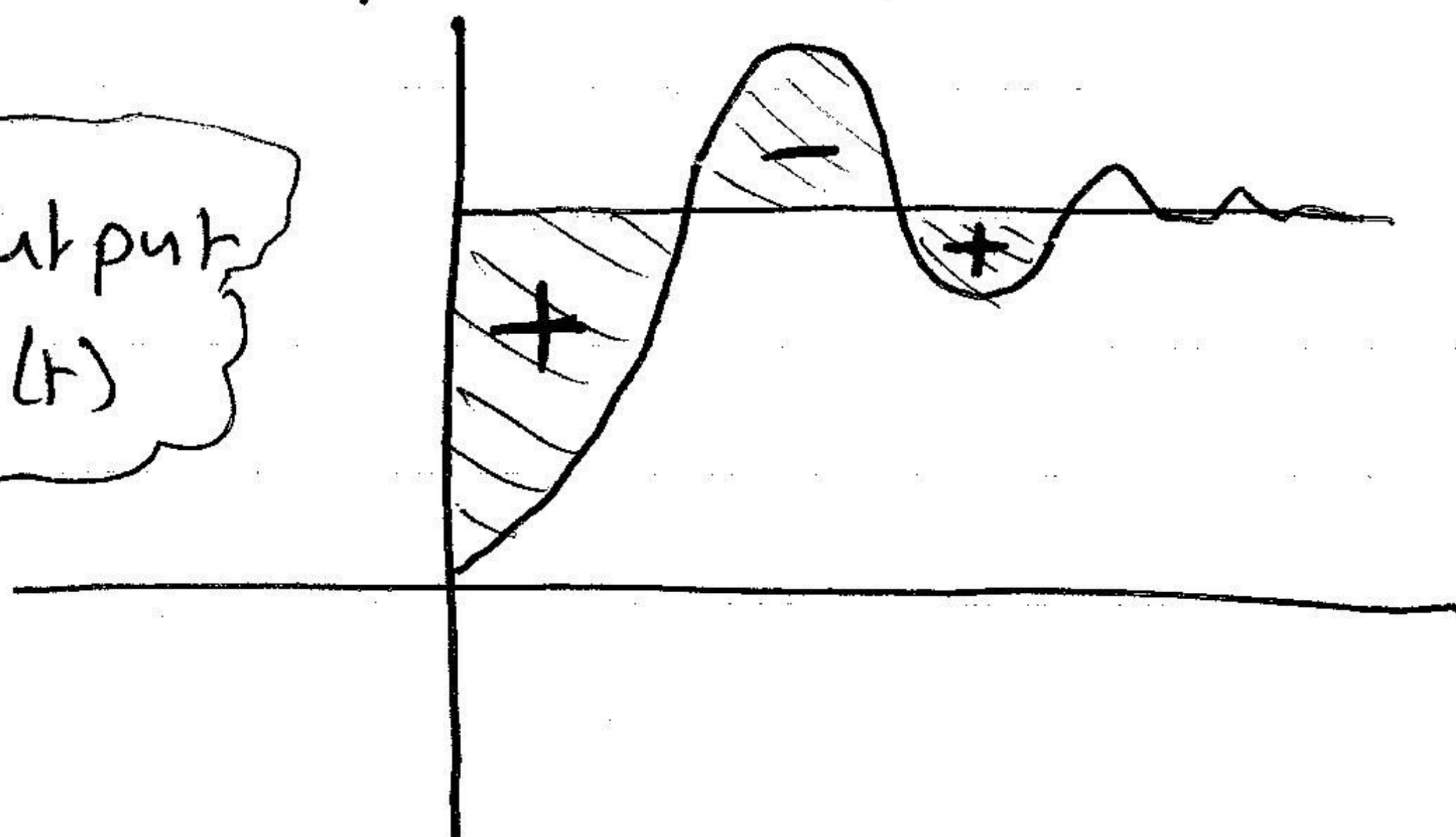
Performance Index Symbol : $[I]$



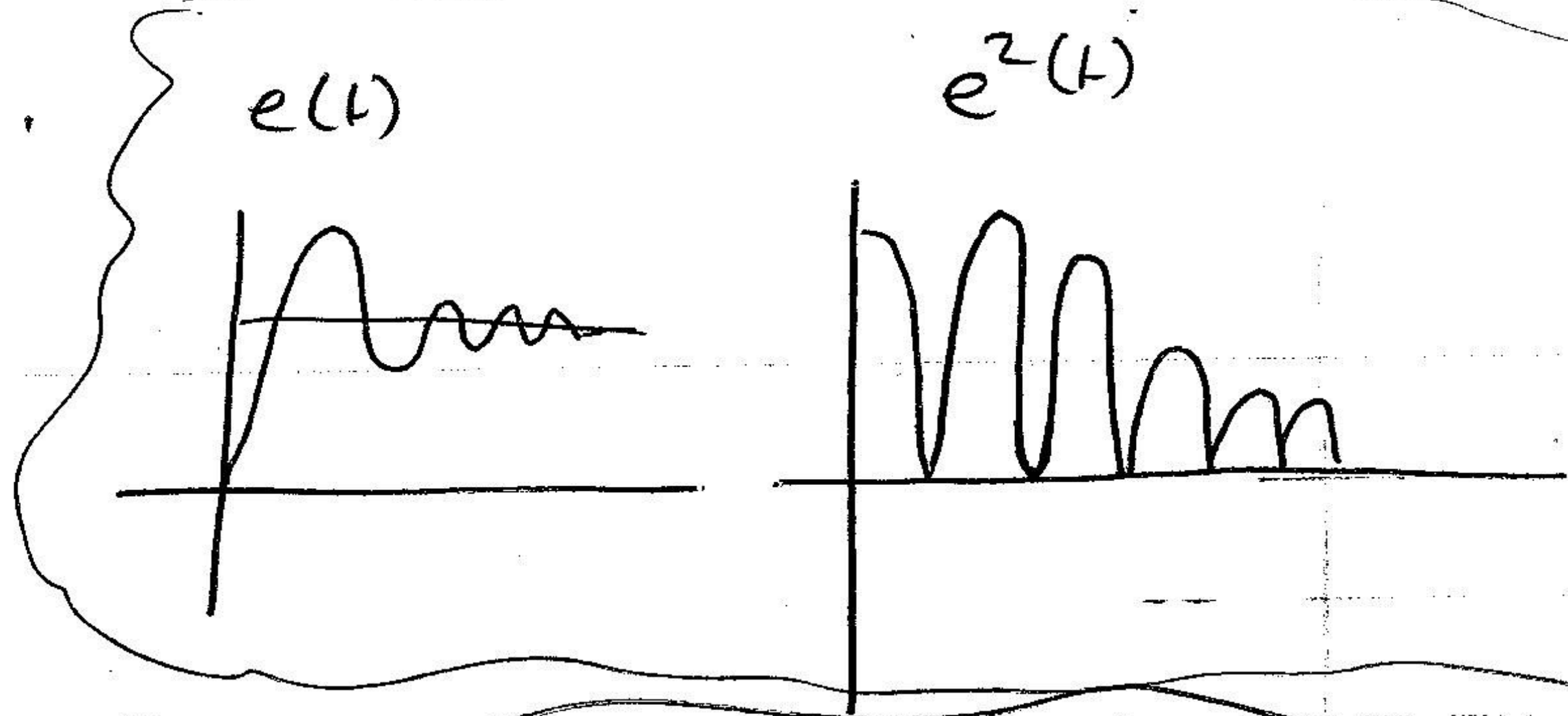
Error Criterion J -

1. Integral of the Square of the error (ISE)

$$\text{error} = \text{Input} - \text{output} \\ = R(t) - C(t)$$

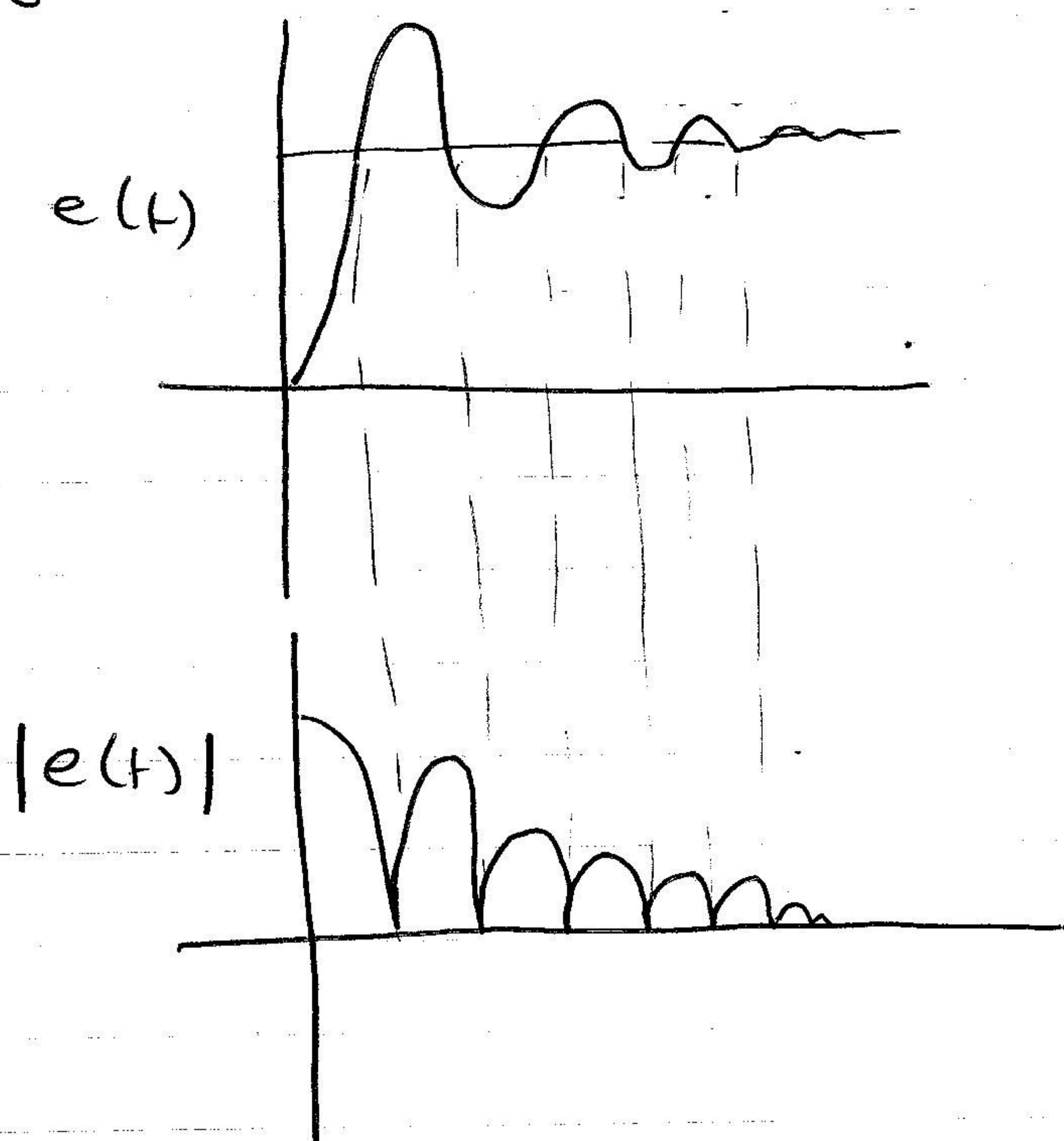


$$I = \int_0^{T_s (T_s \text{ or } \infty)} e^2(t) \cdot dt$$



2. Integral of the absolute value of the error (IAE)

$$I = \int_0^{T_s (T_s \text{ or } \infty)} |e(t)| dt$$



3. Integral of time multiplied by absolute error (ITAE)

$$I = \int_0^{T_s (T_s \text{ or } \infty)} t |e(t)| dt$$

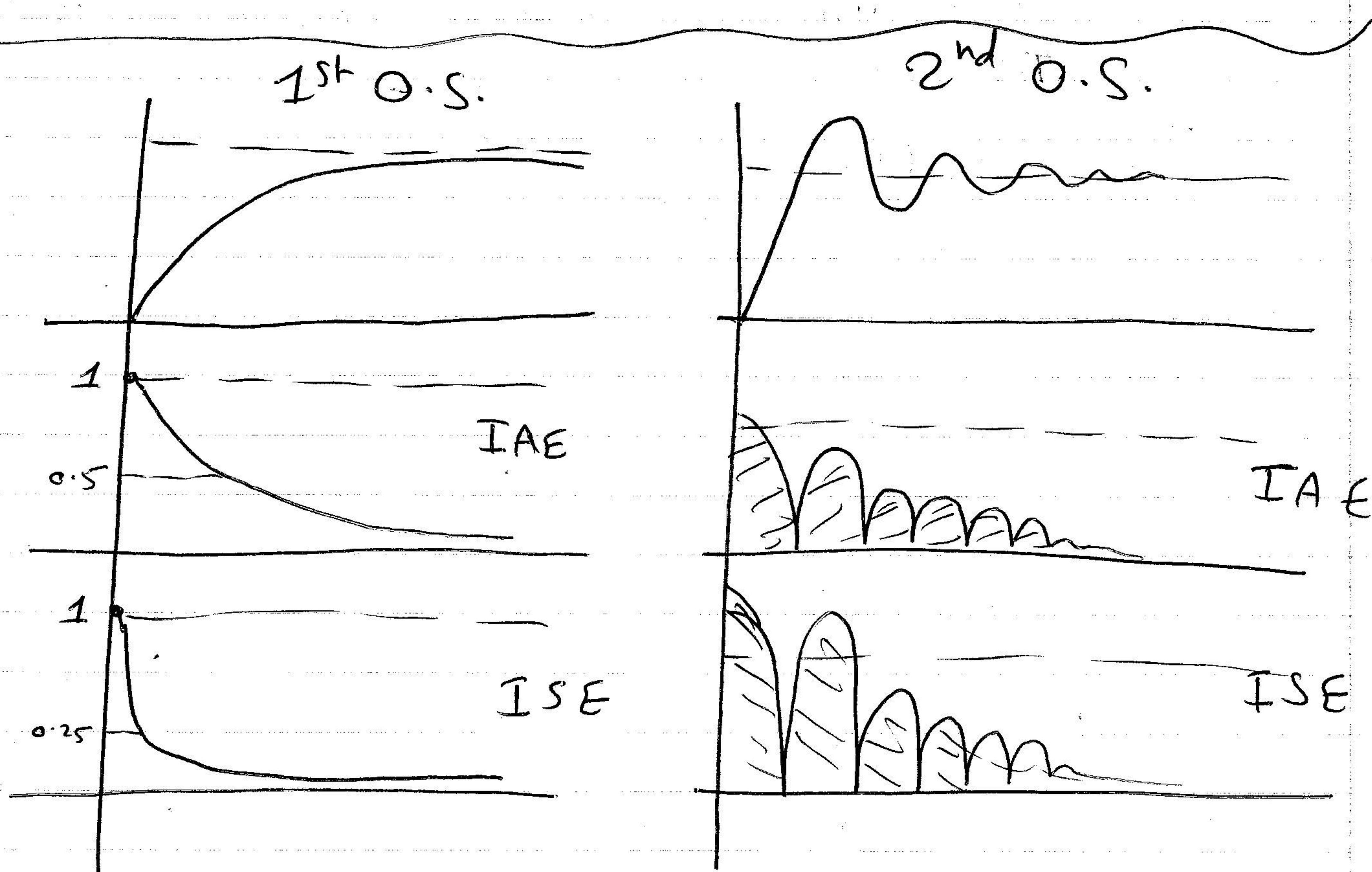
to reduce the contribution of ~~initial~~ Initial error,

$t = \infty$
 $e = 0$

75

4. Integral of time multiplied by square error (ITSE)

$$I = \int_0^{T_s} t e^2(t) dt$$

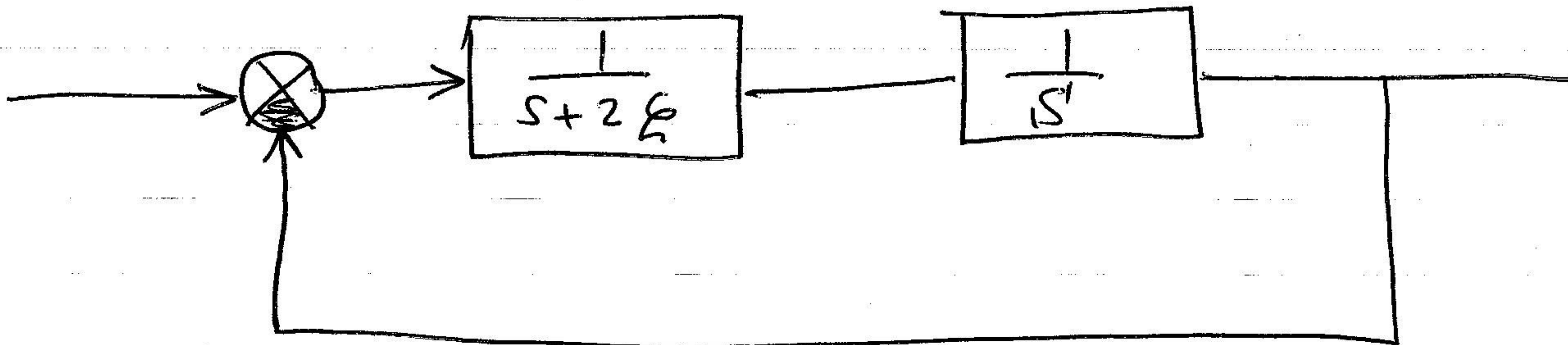


Example

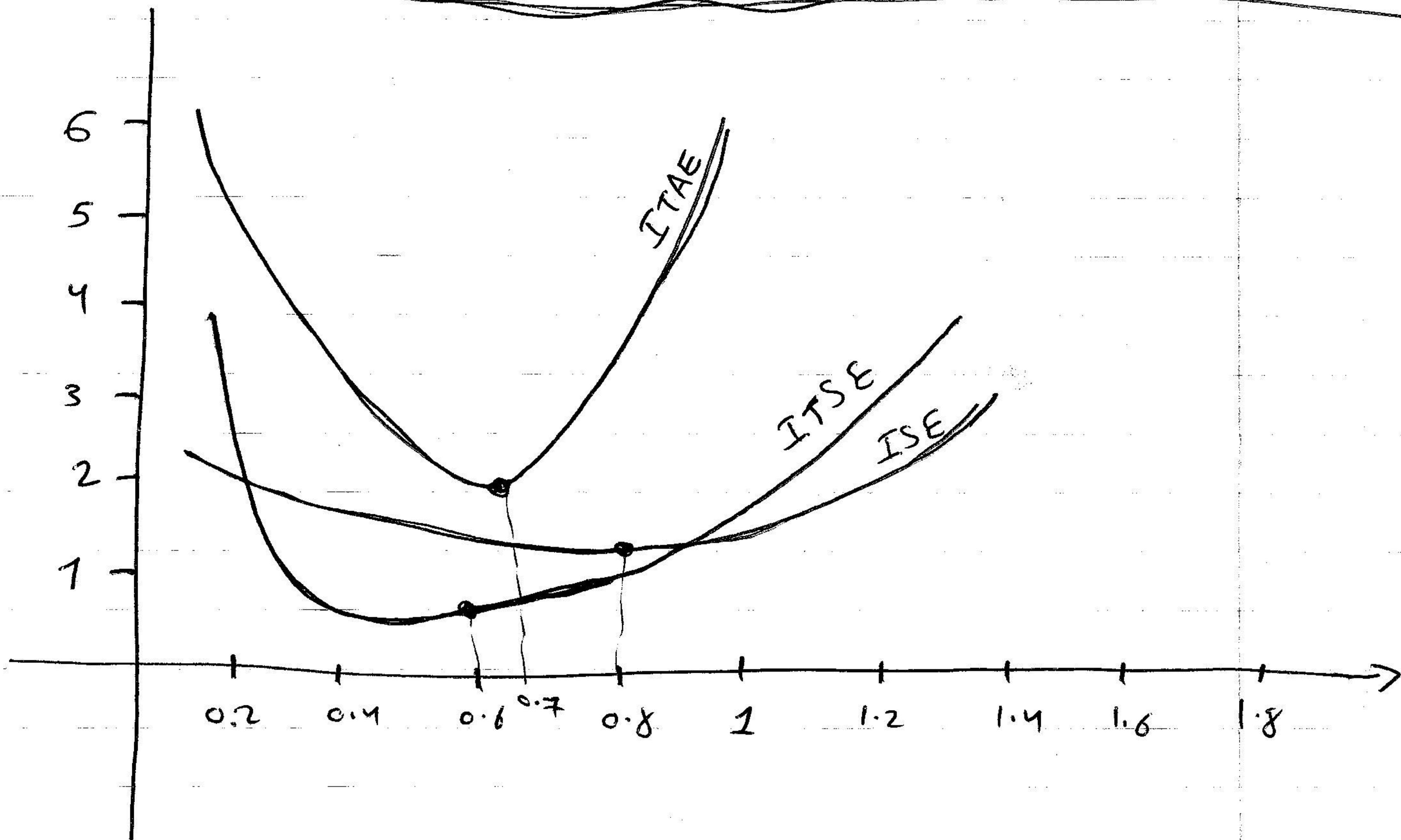
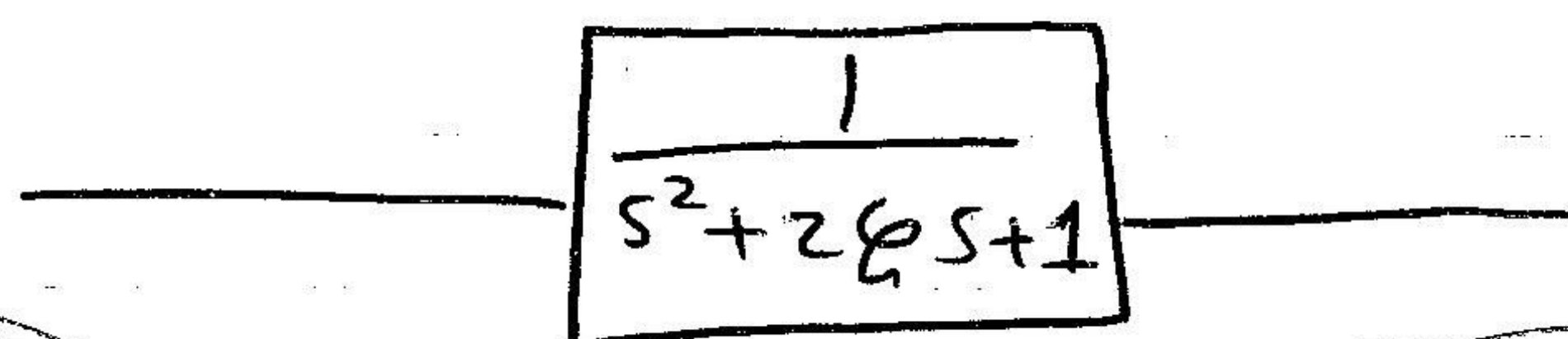
a single loop feedback control system is shown below
where W_n is normalized ($W_n=1$).

find the value of (ξ) so that the system is called
optimum controlled.





|||



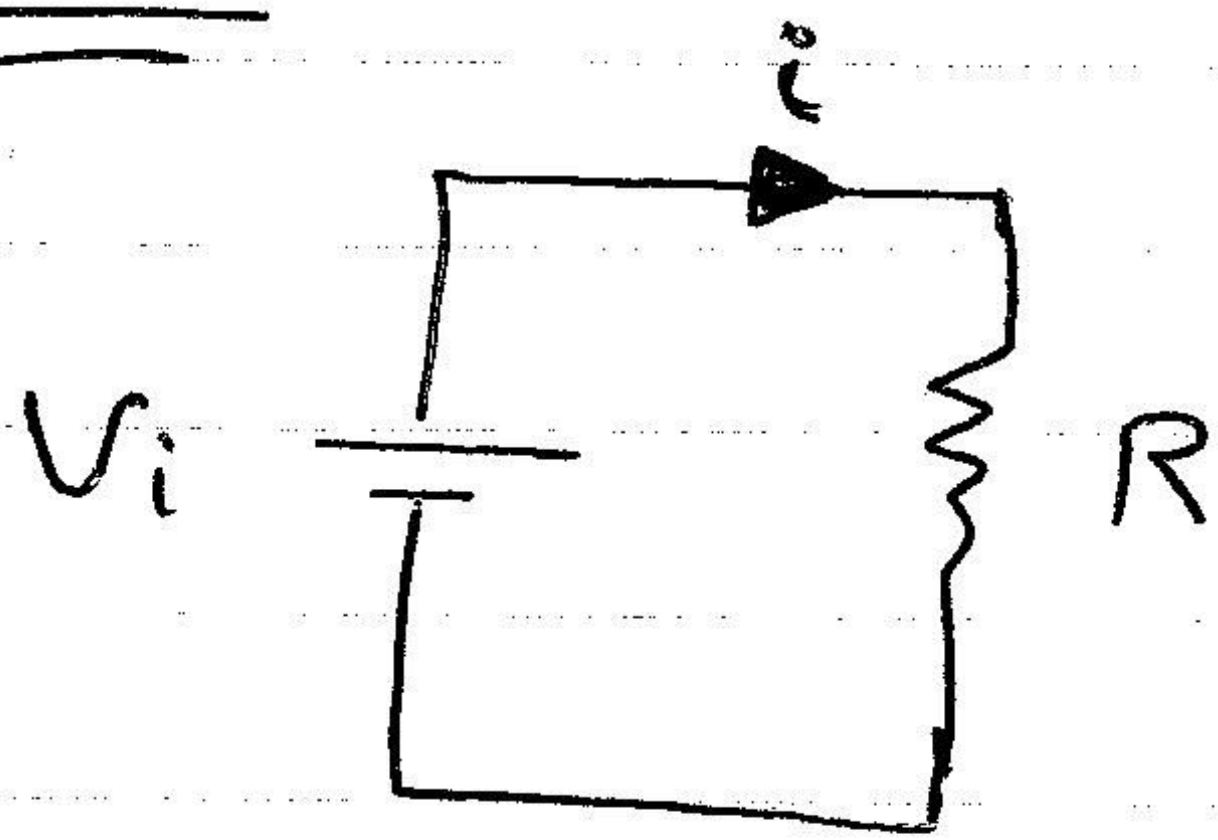
- ⊗ Optimal Value of ζ based on ITAE = $\boxed{0.7}$ ✓ ζ
- ⊗ optimal Value of ζ based on ITSE = $\boxed{0.6}$
- ⊗ optimal Value of ζ based on ISE = $\boxed{0.8}$

Control

Linear

Non-linear

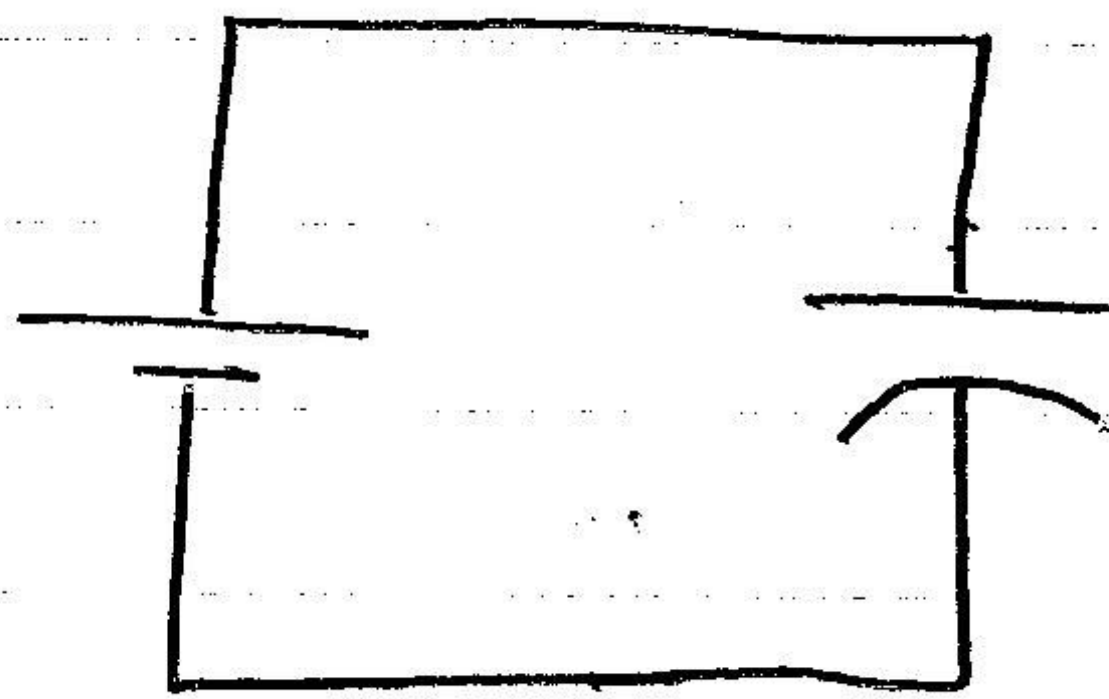
(Linear)



$$V = IR$$

$$V(s) = I(s) * R$$

(Linear)

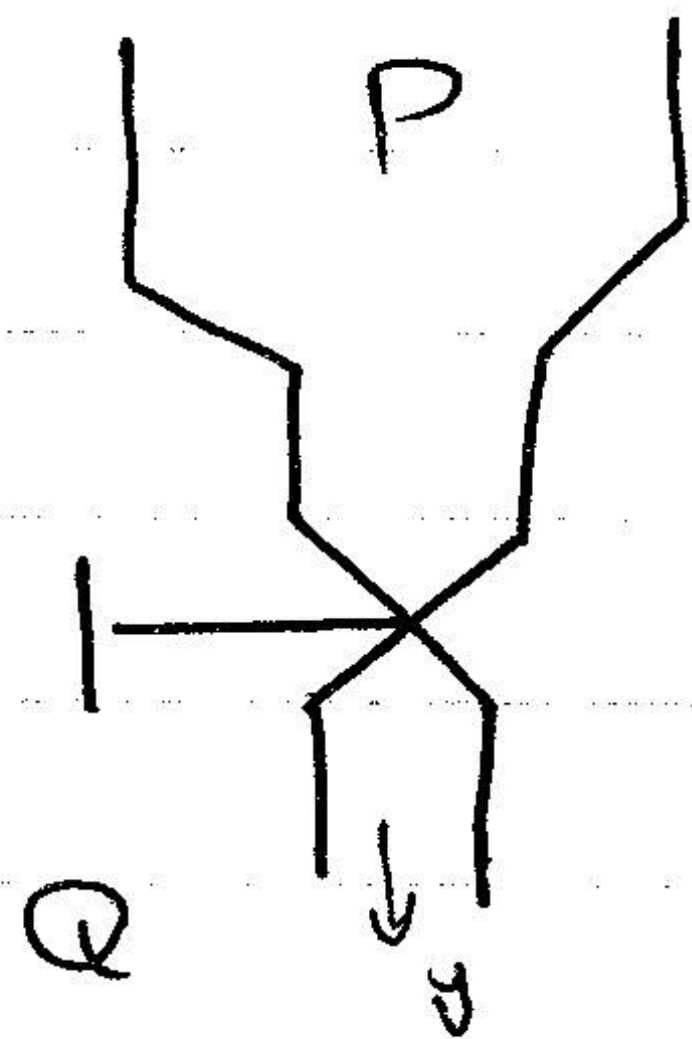


$$V = \frac{1}{C} \int i \, dt$$

$$V(s) = \frac{1}{C} \frac{I(s)}{s}$$

(Linear)

(Non-Linear)



$$Q = \frac{P}{R}$$

$$P = \rho g h$$

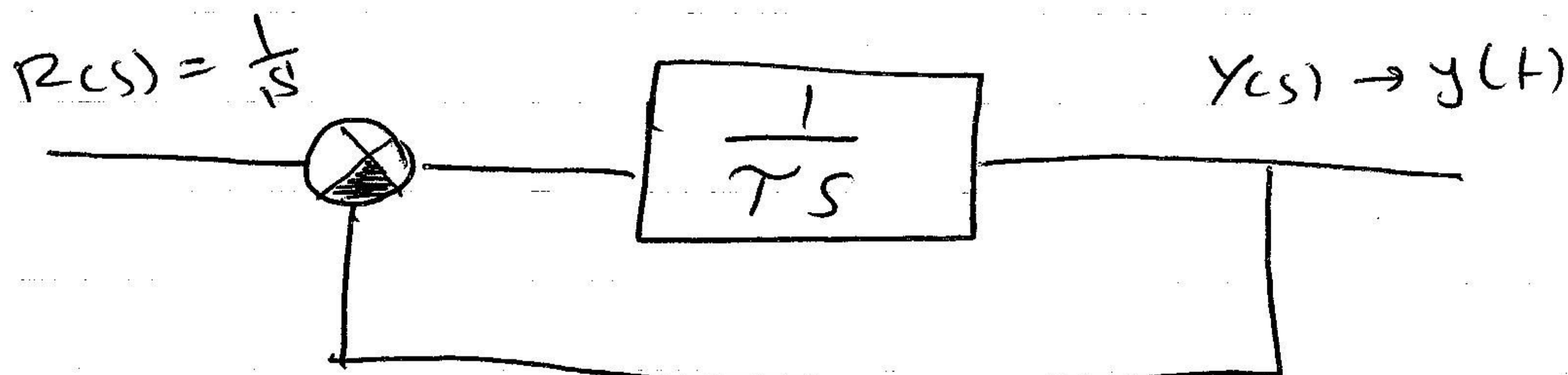
$$Q \propto \sqrt{\Delta P}$$

In Control 2, We Study linear Control Systems only!

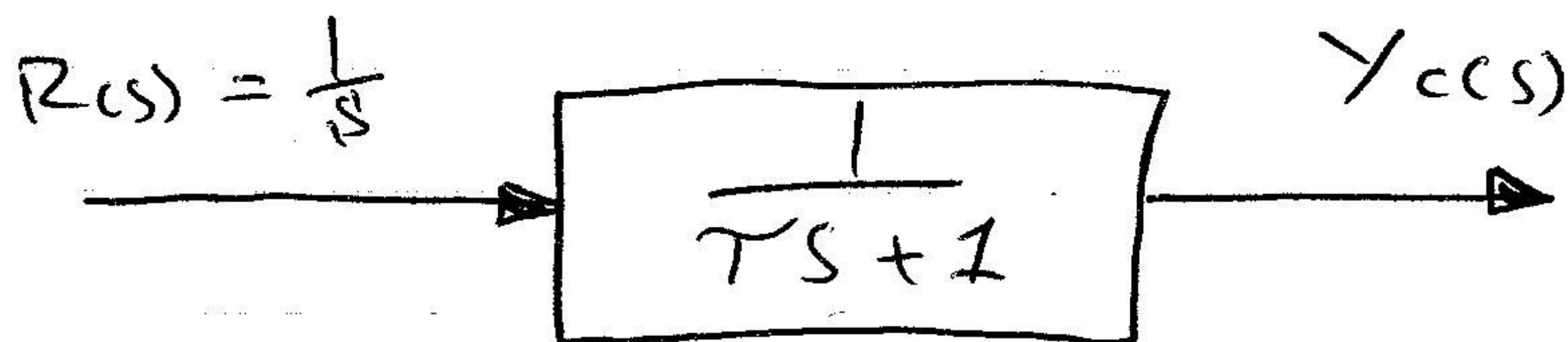
Continue :

Ex For the following system, find the performance Index based on IAE, ISE, ITAE, ITSE.

Note : Performance Index based on time domain.



|||



$$y(t) = 1 - e^{-t/\tau}$$

$$e(t) = r(t) - y(t) = \boxed{e^{-t/\tau}}$$

$$\begin{aligned} \boxed{1.} \quad I_{IAE} &= \int_0^{\infty} |e^{-t/\tau}| dt = \int_0^{\infty} e^{-t/\tau} dt \\ &= \frac{e^{-t/\tau}}{-1/\tau} = -\tau e^{-t/\tau} \Big|_0^{\infty} \\ &= 0 - (-\tau) = \boxed{\tau} \end{aligned}$$

$$\boxed{2.} \quad I_{ISE} = \int_0^{\infty} (e^{-t/\tau})^2 dt = \int_0^{\infty} e^{-2t/\tau} dt$$

$$= \int_0^{\infty} e^{-t/\tau} dt = \boxed{\frac{\tau}{2}}$$

$$\boxed{3.} \quad I_{ITAE} = \int_0^{\infty} t |e^{-t/\tau}| dt$$

$$= \int_0^{\infty} t e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} - \int -\tau e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} + \tau \int e^{-t/\tau} dt$$

$$= -\tau t e^{-t/\tau} - \tau^2 e^{-t/\tau} \Big|_0^{\infty}$$

$$= [0 - 0] - [0 - \tau^2] = \boxed{\tau^2}$$

$$\boxed{4.} \quad I_{ITSE} = \int_0^{\infty} t (e^{-t/\tau})^2 dt = \int_0^{\infty} t e^{-2t/\tau} dt$$

Suppose $L = \tau/2$

$$\therefore \int_0^{\infty} t e^{-t/L} dt \quad \left(\begin{array}{c} \uparrow \\ \text{نفس حل القسم الثالث أعلاه} \end{array} \right)$$

$$\therefore \int_0^{\infty} t e^{-t/L} dt = \boxed{\tau^2} L^2$$

but $L = \tau/2$

$$\therefore \text{Answer} = \boxed{\frac{\tau^2}{4}}$$

Back to Sensitivity

There is a mathematical Method to compute \sqrt{x} .

Ex We need to find $\sqrt{5}$

Solution

$$y = \sqrt{x}$$

$$\frac{dy}{dx} = \frac{1}{2\sqrt{x}}$$

$$\frac{\Delta y}{\Delta x} = \frac{1}{2\sqrt{x_0}}$$

$$\Delta y = \frac{1}{2\sqrt{x_0}} * \Delta x = \frac{1}{2\sqrt{4}} * 1 = \frac{1}{4} * 1 = \frac{1}{4}$$

$$= 0.25$$

$$\therefore \sqrt{5} = y + \Delta y = 2 + 0.25 = 2.25$$

$$y_0 = \sqrt{x_0}$$

$$2 = \sqrt{4}$$

$$y_0 + \Delta y = \sqrt{5}$$

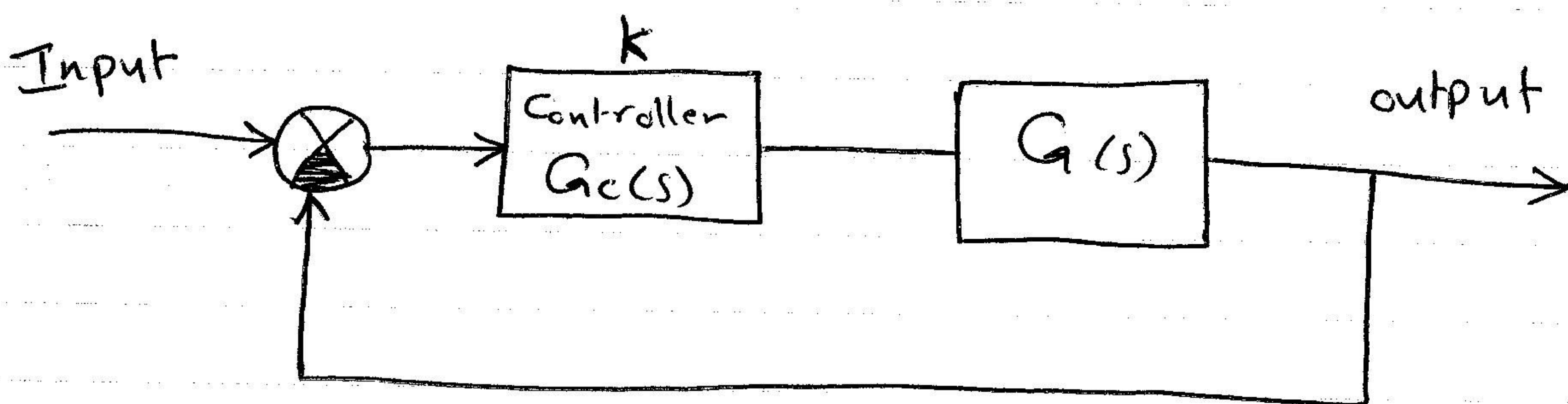
$$2 + \Delta y = \sqrt{5}$$

$$dx = 1 \approx \Delta x$$

System Sensitivity : is the ratio of change in the System transfer function to the change of a process transfer function (or parameter) for a small incremental change.

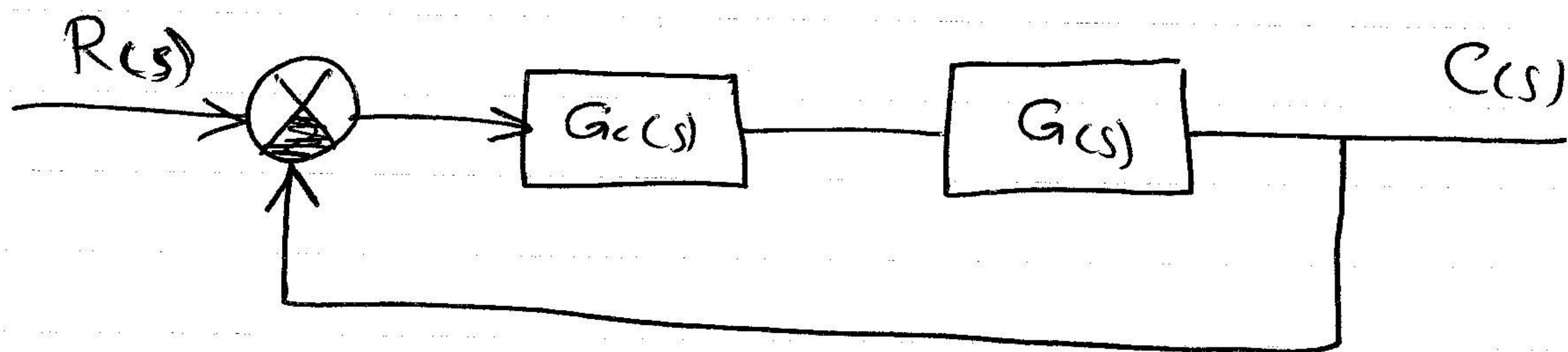
$$T(s) = \frac{Y(s)}{R(s)}$$

$$S_G^T = \frac{dT/T}{dG/G} = \frac{d \ln T}{d \ln G}$$



$$S_G^T = \frac{dT/T}{dG/G} = \frac{d \ln T}{d \ln G} = \frac{dT}{dG} \cdot \frac{G}{T}$$

Ex For the following system, find the Sensitivity of the system to process.



$$T(s) = \frac{G_c G}{1 + G_c G}$$

⇒

$$S_G^T = \frac{dT}{dG} * \frac{G}{T}$$

$$\Rightarrow \frac{dT}{dG} = \frac{(1+G_c G) G_c - G_c G G_c}{(1+G_c G)^2}$$

~~$$\frac{G_c}{(1+G_c G)^2}$$~~

$$= \frac{G_c + G_c^2/G - G_c^2/G}{(1+G_c G)^2}$$

$$= \boxed{\frac{G_c}{(1+G_c G)^2}}$$

~~$$\frac{dT}{dG}$$~~

$$S_G^T = \frac{dT}{dG} * \frac{G}{T} = \frac{G_c}{(1+G_c G)^2} * \frac{G}{\frac{G_c G}{1+G_c G}}$$

$$= \frac{1+G_c G}{(1+G_c G)^2} = \boxed{\frac{1}{1+G_c G}}$$

* For the upper system, find the sensitivity of the system to feed back.

$$S_H^T = \frac{dT}{dH} * \frac{H}{T}$$

$$T(s) = \frac{G_c G}{1 + G_c G H}$$

$$\frac{dT}{dH} = \frac{(1 + G_c G H)(0) - (G_c G)(G_c G)}{(1 + G_c G H)^2}$$

$$= \frac{-G_c^2 G^2}{(1 + G_c G H)^2}$$

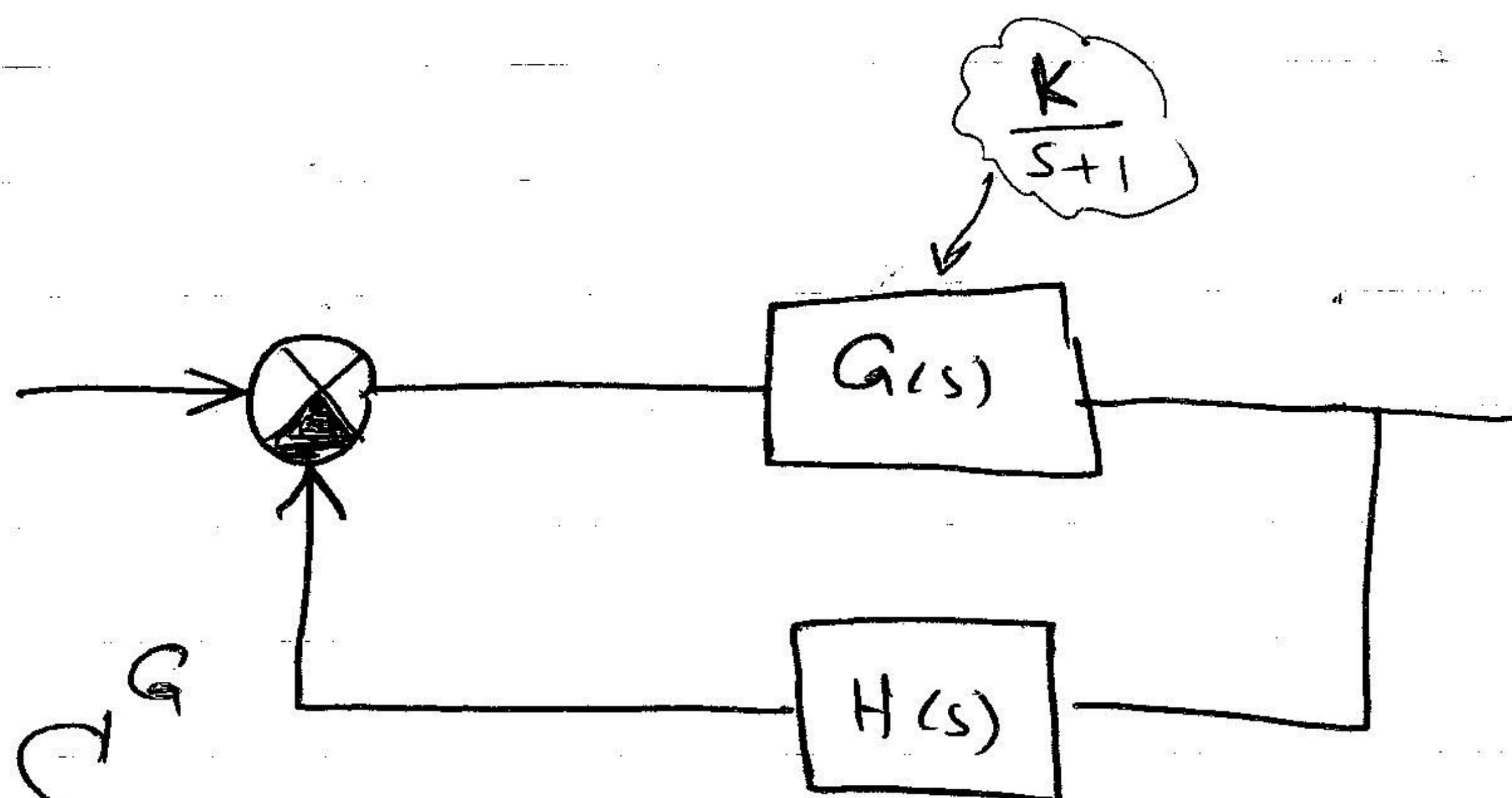
$$\therefore S_H^T = \frac{dT}{dH} * \frac{H}{T} = \frac{-G_c^2 G^2}{(1 + G_c G H)^2} * \frac{H}{\frac{G_c G}{1 + G_c G H}}$$

$$= \boxed{\frac{-G_c G H}{1 + G_c G H}}$$

Chain Rule

$$S_{\alpha}^T = S_G^T * S_{\alpha}^G$$

for example:



$$S_K^T = S_G^T * S_K^G$$

$$T.F. = \frac{G}{1+GH}$$

$$\textcircled{1} S_G^T = \frac{dT}{dG} * \frac{G}{T} = \frac{1+GH - GH}{(1+GH)^2} * \frac{G}{1+GH}$$

$$= \boxed{\frac{1}{1+GH}}$$

$$\textcircled{2} S_K^G = \frac{dG}{dk} * \frac{k}{G}$$

$$G = \frac{k}{s+1}$$

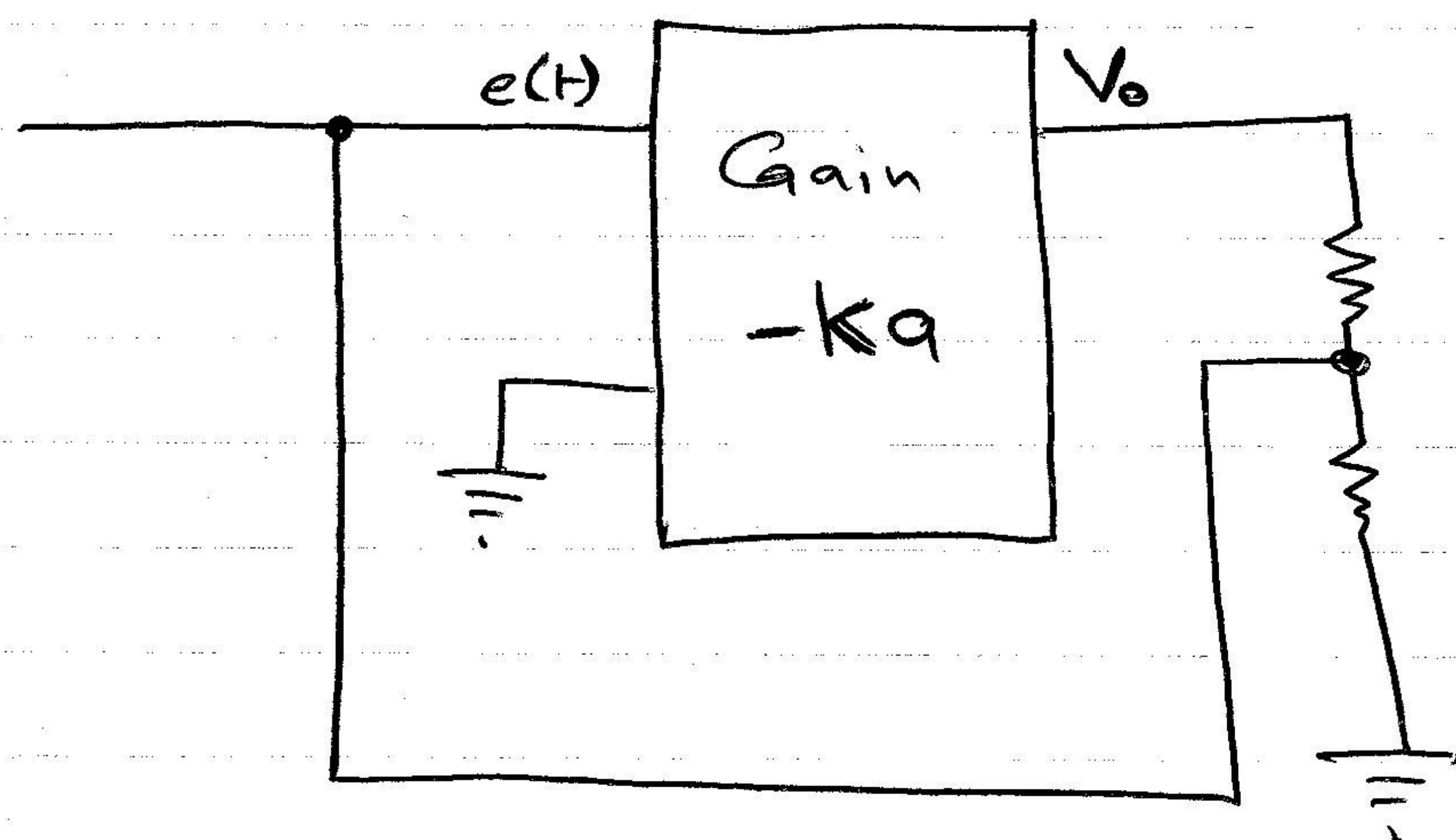
$$\therefore S_K^G = \frac{dG}{dk} * \frac{k}{G} = \frac{1}{s+1} * \frac{k}{\frac{k}{s+1}} = 1 * 1 = \boxed{1}$$

$$\Rightarrow \therefore S_K^T = S_G^T * S_K^G = \frac{1}{1+GH} * 1 = \boxed{\frac{1}{1+GH}}$$

Example :- Feed back Amplifier

Find the sensitivity of the system to $|k_a|$

$\therefore \frac{d|k_a|}{|k_a|}$
 $S_{k_a}^T$



$$\beta = \frac{R_2}{R_1 + R_2}$$

$$e(t) = V_{in} + \frac{V_o * R_2}{R_1 + R_2} \quad \text{--- (1)}$$

$$V_o = e(t) * -k_a \quad \text{--- (2)}$$

$$e(t) = V_{in} + \frac{V_o * R_2}{R_1 + R_2} ; \quad \text{divide } \frac{V_o * R_2}{R_1 + R_2} \text{ on } R_1$$

$$\therefore e(t) = V_{in} + \frac{V_o \beta}{1 + \beta} \quad \text{--- (1) } * *$$

$$V_o = e(t) * -k_a \quad \text{--- (2)}$$

From (1) and (2) :-

$$V_o = \left[V_{in} + \frac{\beta}{\beta + 1} V_o \right] * -k_a$$

$$\Rightarrow V_o = -k_a V_{in} - \frac{\beta}{\beta+1} k_a V_o$$

$$\Rightarrow V_o + \frac{\beta}{\beta+1} k_a V_o = -k_a V_{in}$$

$$\Rightarrow \boxed{\frac{V_o}{V_{in}} = \frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}}$$

$$\therefore T = \frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}$$

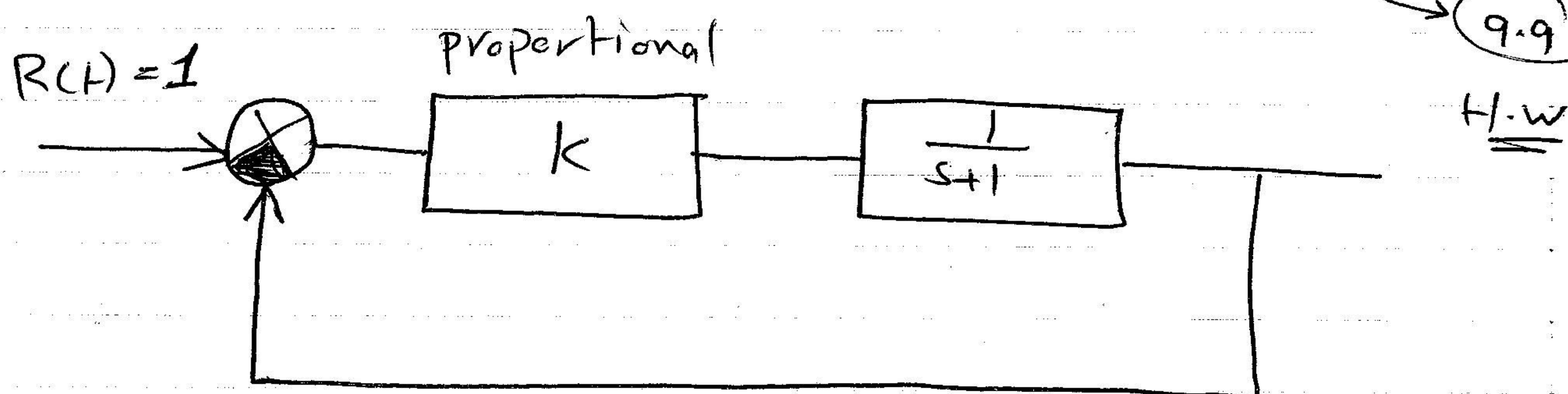
$$S_{k_a}^T = \frac{dT}{dk_a} * \frac{k_a}{T}$$

$$\frac{dT}{dk_a} = \frac{(1 + \frac{\beta}{\beta+1} k_a)(-1) - (-k_a)(\frac{\beta}{\beta+1})}{(1 + \frac{\beta}{\beta+1} k_a)^2}$$

$$\therefore S_{k_a}^T = \frac{(1 + \frac{\beta}{\beta+1} k_a)(-1) + (k_a)(\frac{\beta}{\beta+1})}{(1 + \frac{\beta}{\beta+1} k_a)^2} * \frac{k_a}{\frac{-k_a}{1 + \frac{\beta}{\beta+1} k_a}}$$

$$\approx \boxed{\frac{1}{1 + \frac{\beta}{\beta+1} k_a}}$$

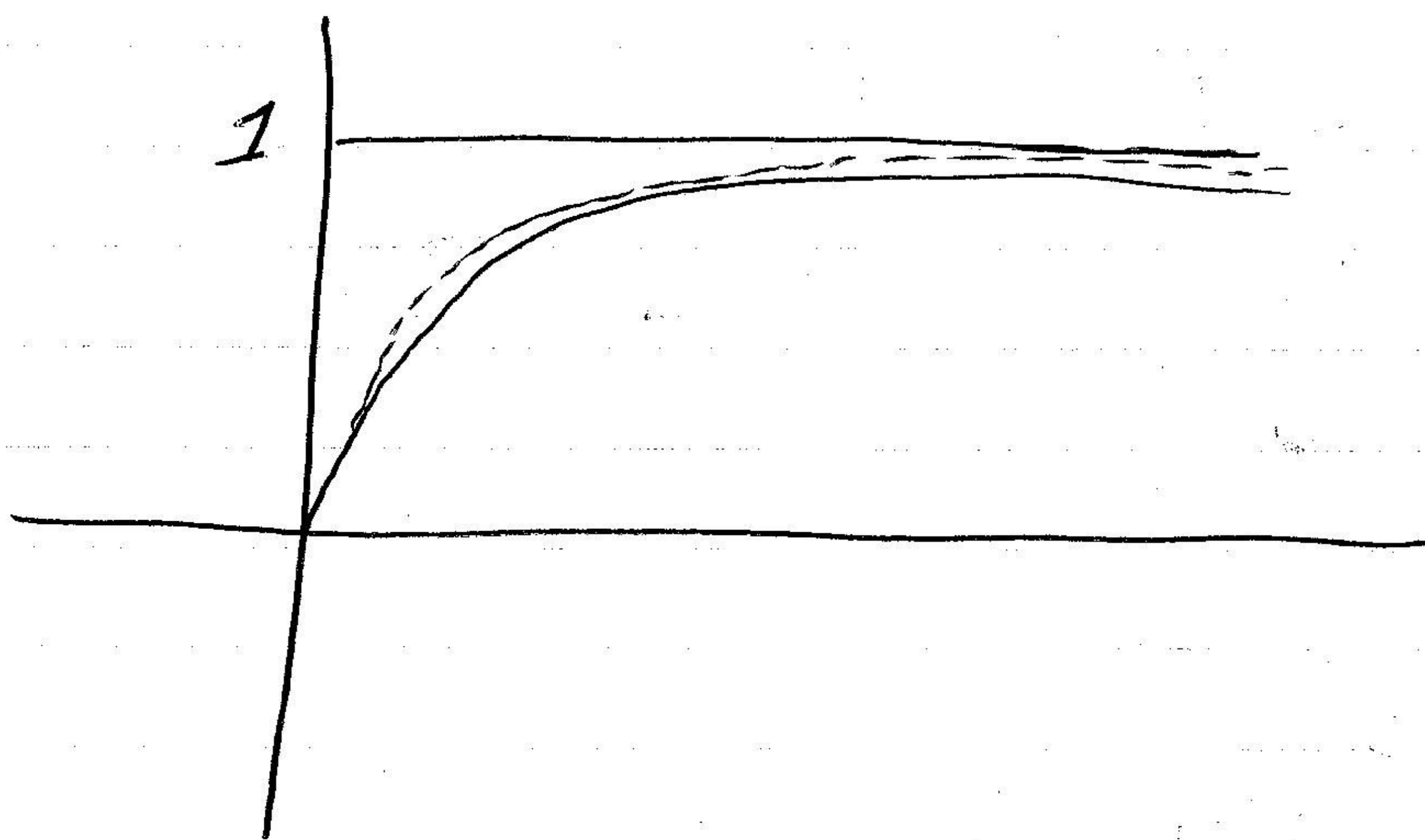
Ex :- For the following example, find the response of the system as k varies from 10 to 11



$$Y_{ss} = \frac{k}{1+k} R$$

$$Y_{ss} \Big|_{k=10} = \frac{10}{1+10} * 1 = \frac{10}{11} = \boxed{0.909}$$

$$Y_{ss} \Big|_{k=11} = \frac{11}{1+11} * 1 = \frac{11}{12} = \boxed{0.916}$$



$$S_k^T = \frac{dT}{dk} * \frac{k}{T}$$

$$T(s) = \frac{kG}{1+kG}$$

$$\therefore S_k^T \approx \frac{dT}{dk} * \frac{k}{T}$$

$$= \frac{(1+kG)G - kG * G}{(1+kG)^2} * \frac{k}{kG}$$

$$= \boxed{\frac{-1}{1+kG}}$$

$$= \frac{1}{1 + \frac{k}{s+1}}$$

$$\boxed{\frac{s+1}{s+1+k}}$$

~~$$\frac{s+1}{s+1+k}$$~~

⊗ at static response $\Rightarrow S=0$

$$S_k^T = \frac{0+1}{0+1+k} = \boxed{\frac{1}{1+k}}$$

~~$$\frac{s+1}{s+1+k}$$~~

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k} \quad \frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

~~$$\frac{1}{1+k}$$~~

12/17 سوال (إكمال حل المسألة الخاصة بالحاضر الخاصة)

$$S_G^T = \frac{\frac{\Delta T}{T}}{\frac{\Delta G}{G}} \Rightarrow \frac{\Delta T}{T} = S * \frac{\Delta G}{G}$$

$$Y = T * X$$

$$Y_{\text{new}} = (T + \Delta T) X$$

$$Y_n = Y + \Delta T X$$

$$= X T \left(1 + \frac{\Delta T}{T} \right)$$

$$= Y \left(1 + \frac{\Delta T}{T} \right)$$

Back To the previous Question (Page 88) :-

$$S_K^T = \frac{1}{1+k}$$

$$\frac{\Delta T}{T} = S_K^T * \frac{\Delta k}{k}$$

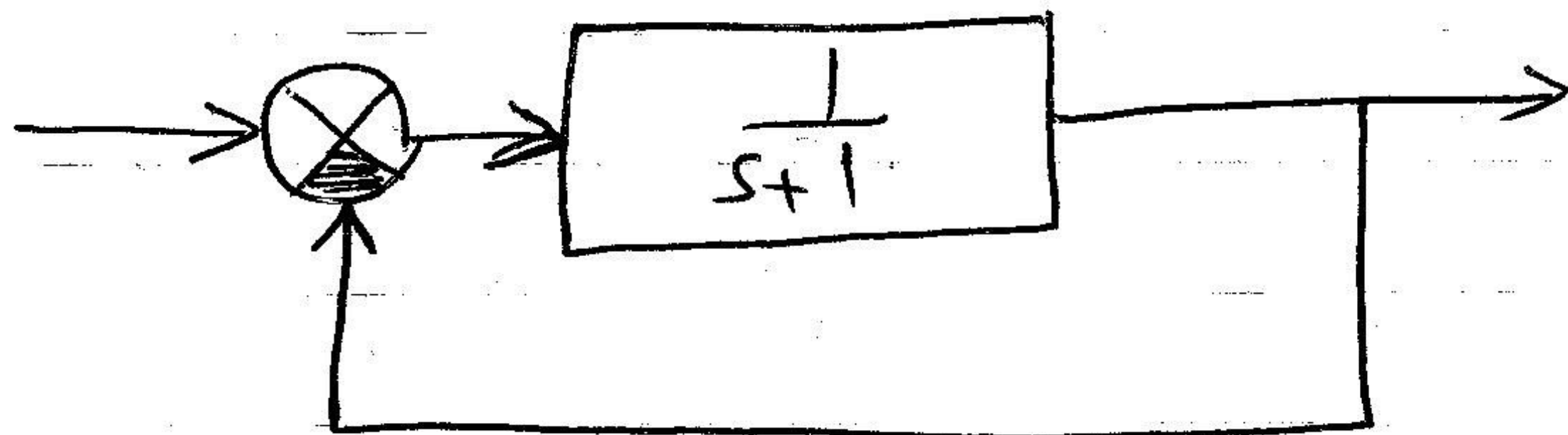
$$= \cancel{\frac{1}{1+10}} * \frac{1}{10} = \frac{1}{11} * \frac{1}{10} = \boxed{\frac{1}{110}}$$

$$Y_n = Y \left(1 + \frac{1}{110} \right)$$

$$= 0.909 \left(1 + \frac{1}{110} \right) = \boxed{0.917}$$

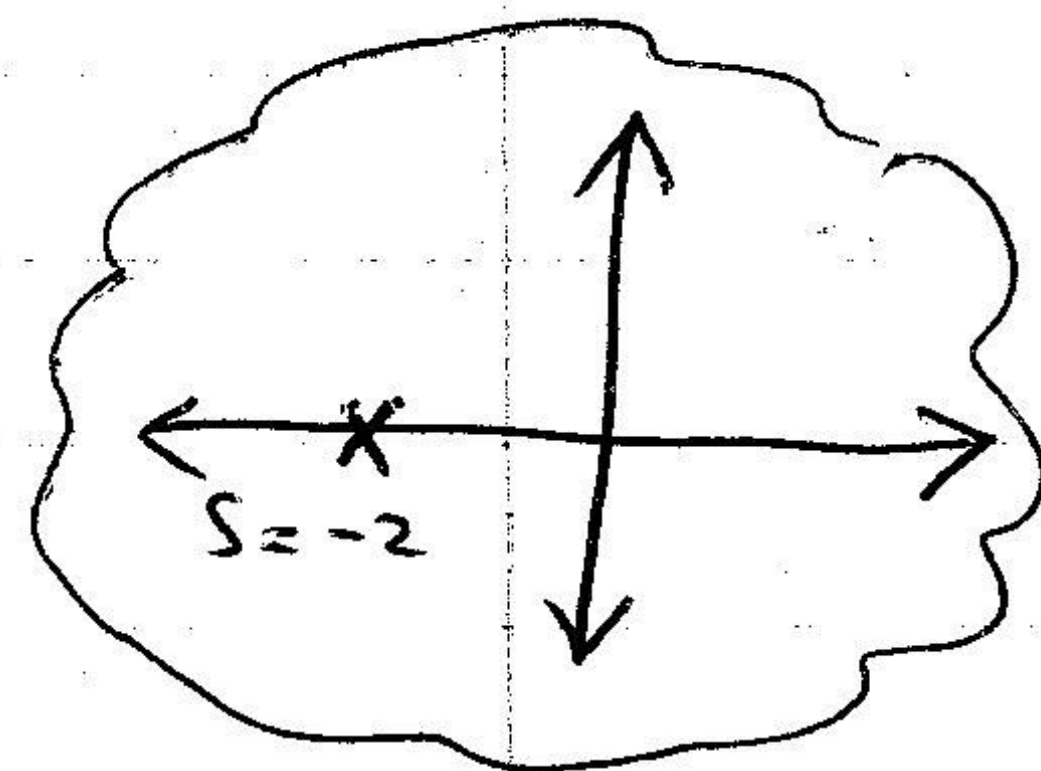
Root Loci

Ex

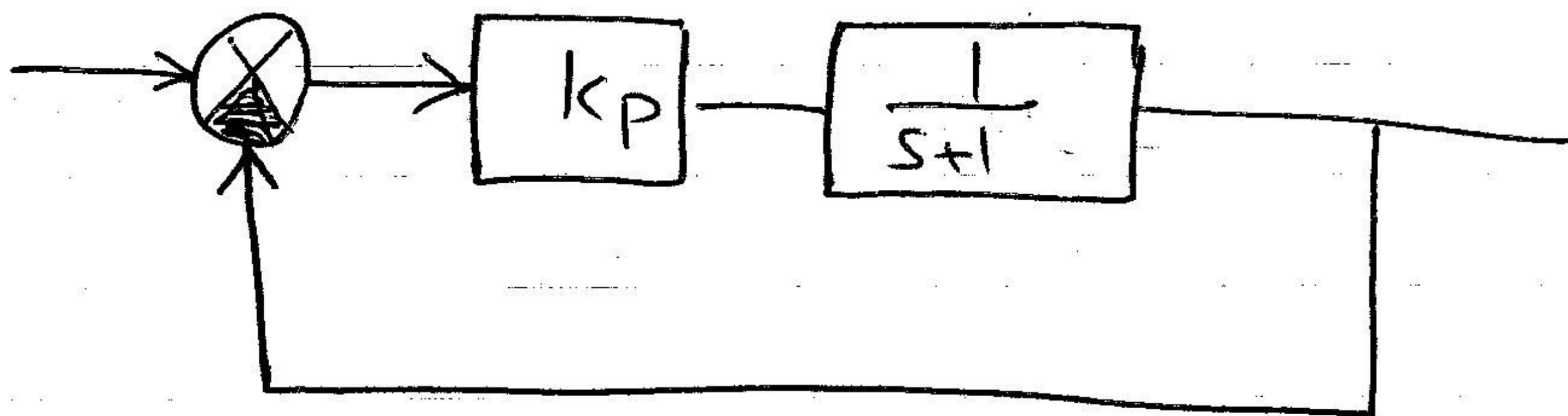


$$T.F. = \frac{1}{s+2}$$

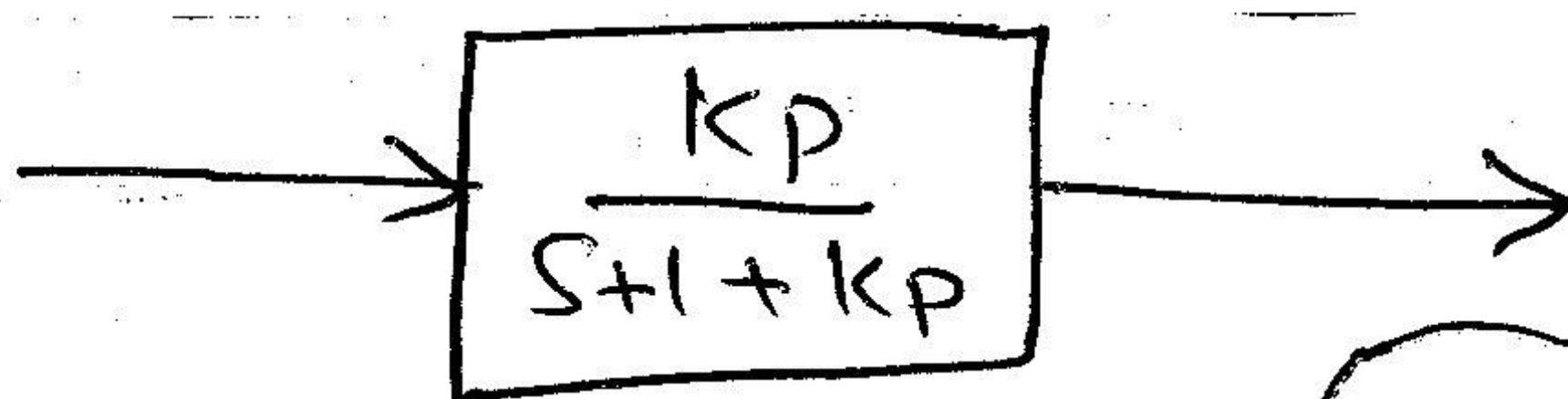
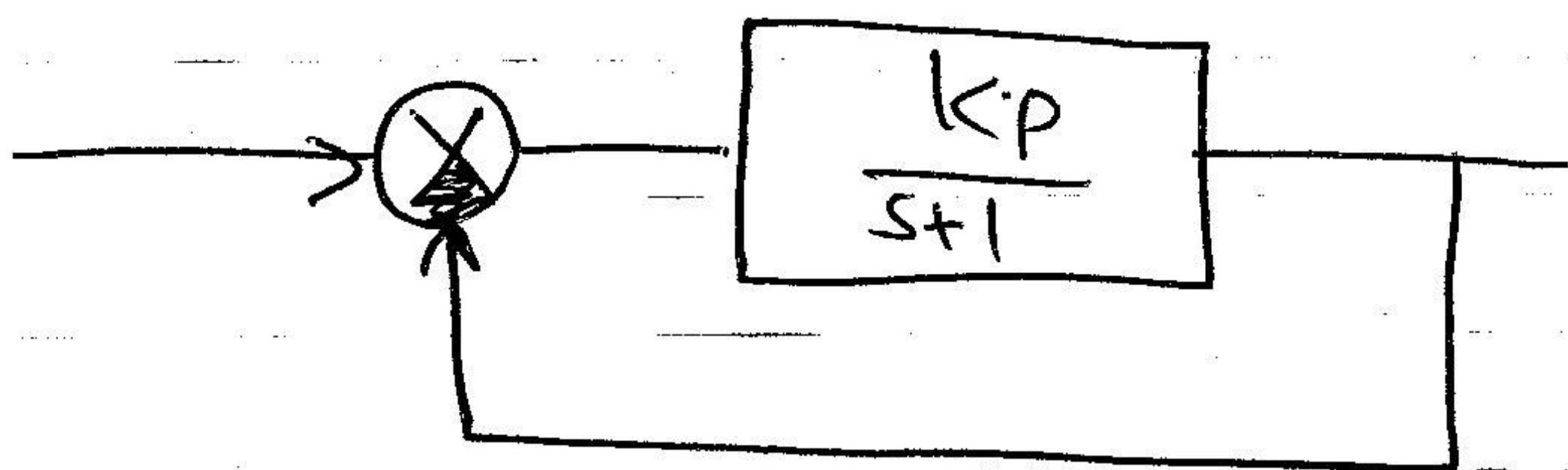
$$q(s) = s+2=0 \Rightarrow \boxed{s=-2} \quad \therefore \text{Stable}$$



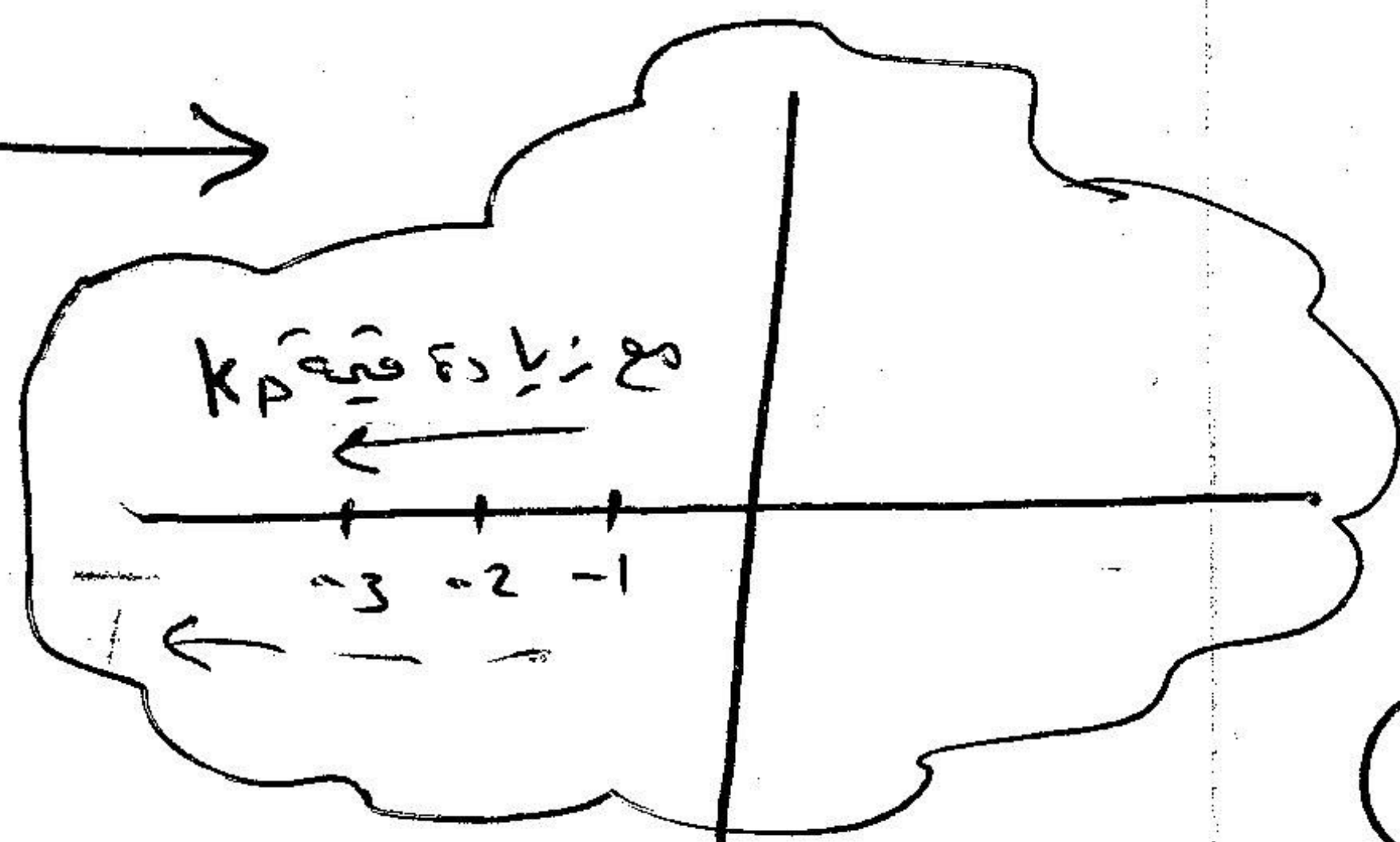
Ex



$$\boxed{K_p = 0 \rightarrow \infty}$$

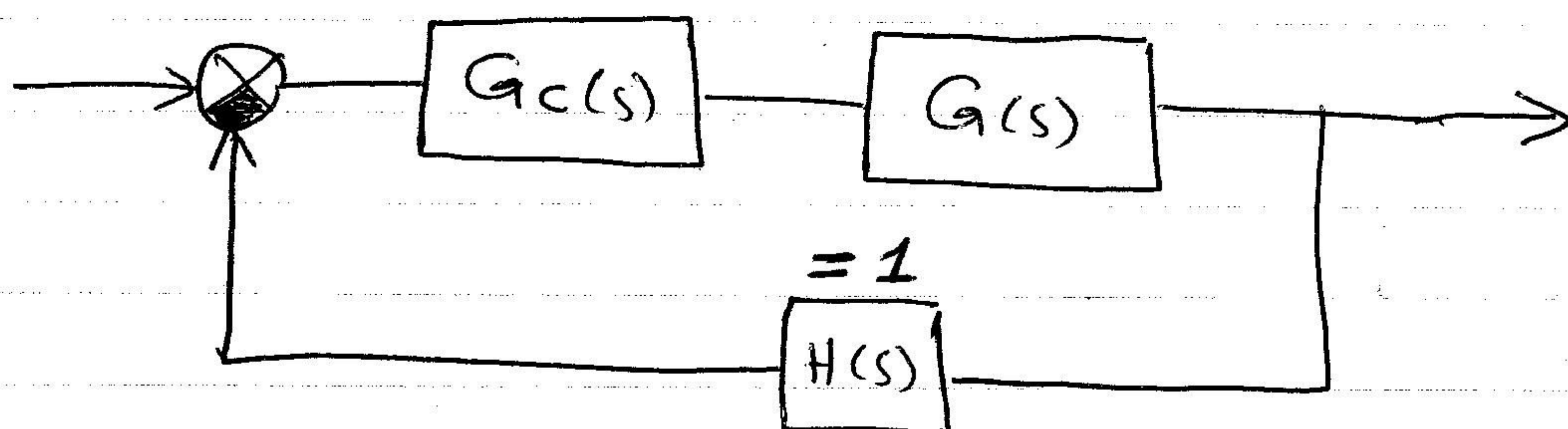


$$\boxed{s = -1 - K_p}$$



Root Loci :- it determines how the roots of characteristic equation move around the s -plane as we change one parameter from $0 \rightarrow \infty$ by a graphical Method.

⊛ This method was introduced by Evans in 1948



$$T(s) = \frac{G_c(s) G(s)}{1 + G_c(s) G(s) H(s)}$$

$$Q(s) = 1 + G_c(s) G(s) H(s)$$

$$Q(s) = 1 + K G(s) = 0$$

$$\Rightarrow K G(s) = -1$$

$$\Rightarrow K G(s) = -1 + j0 = |K G(s)| \angle K G(s) = -1 + j0$$

$$|K G(s)| = 1$$

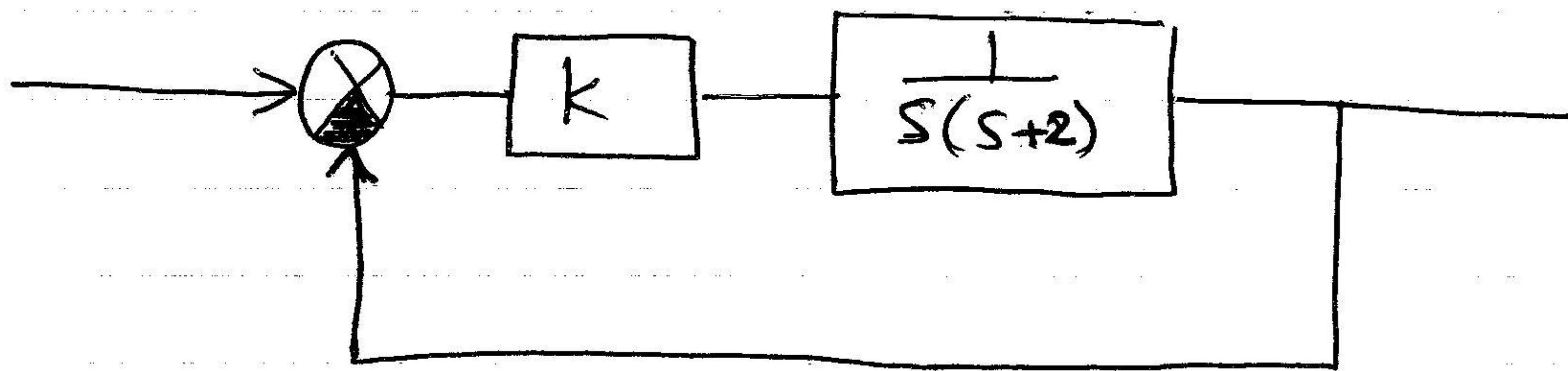
$$\angle K G(s) = 180^\circ \mp k * 360$$

$$k = 1, 2, 3, 4, \dots$$

⇒ We prefer to use angle -180°

⊕ The root locus is the path of the roots of the ch. equ. traced out in s -plane as system parameter is changed from zero \rightarrow infinity.

Ex Find the root locus of the following system.



$$T(s) = \frac{K}{s^2 + 2s + K}$$

as K varies from zero $\rightarrow \infty$

$$\begin{aligned} q(s) &= s^2 + 2s + K = 0 \\ &= s^2 + 2\zeta\omega_n s + \omega_n^2 = 0 \end{aligned}$$

$$s_{1,2} = -\zeta\omega_n \pm \omega_n \sqrt{\zeta^2 - 1}$$

⊕ We want to sketch the function [نقشه]

we will take some points :-

① $K=0 \Rightarrow q(s) = s^2 + 2s = 0 \Rightarrow s(s+2) \Rightarrow s_{1,2} = \underline{\underline{0, -2}}$

② $K=0.5 \Rightarrow q(s) = s^2 + 2s + 0.5 = 0$

$$\Rightarrow s_{1,2} = \frac{-2 \pm \sqrt{4-2}}{2} = -1 \pm \frac{1}{\sqrt{2}} = \boxed{-1 \pm 0.7}$$

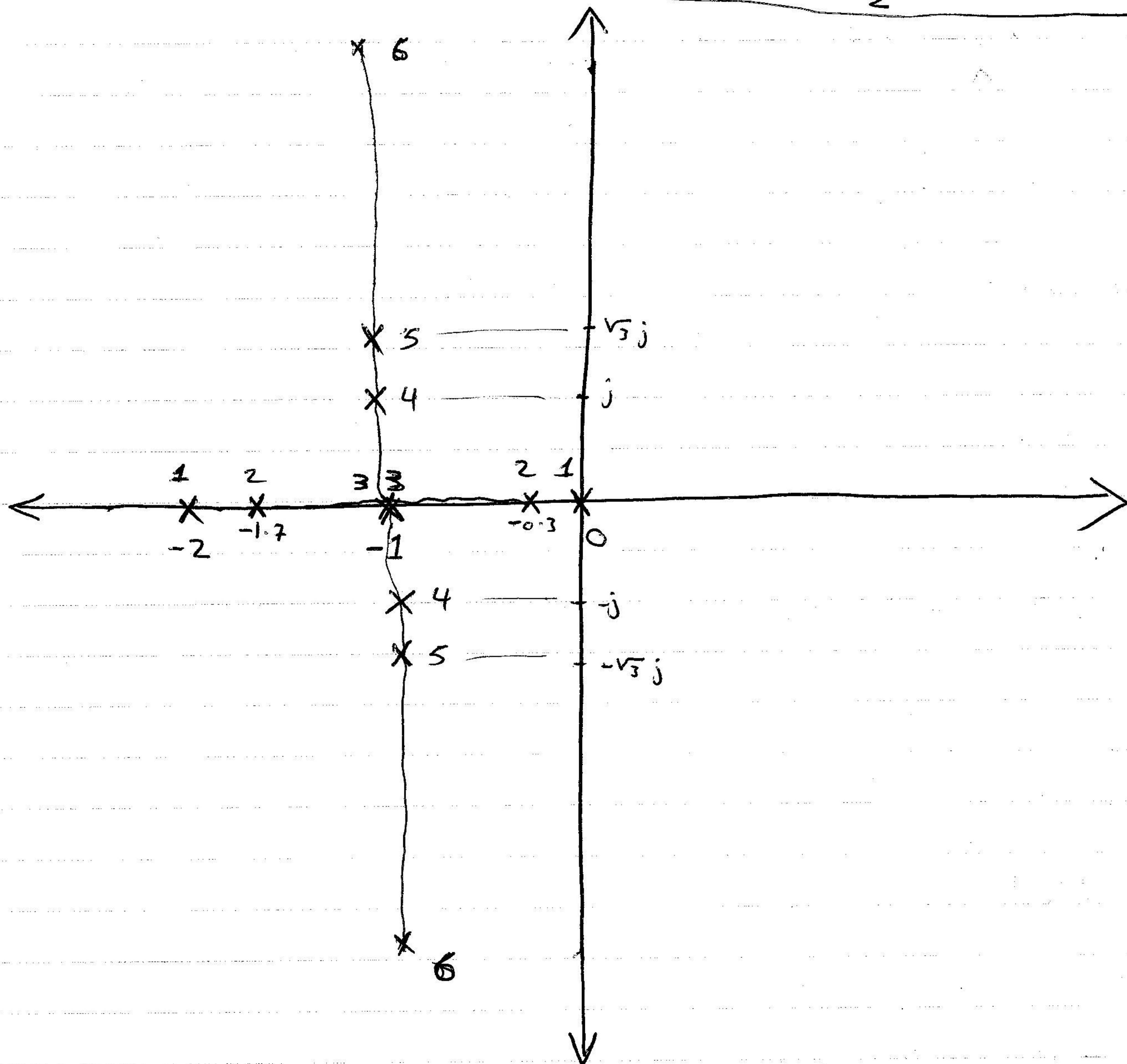
$$\Rightarrow -1 + 0.7 = \boxed{-0.3} \text{ and } -1 - 0.7 = \boxed{-1.7}$$

$$\textcircled{3} \quad k=1 \Rightarrow q(s) = s^2 + 2s + 1 = 0 \Rightarrow s_{1,2} = \boxed{-1}$$

$$\textcircled{4} \quad k=2 \Rightarrow q(s) = s^2 + 2s + 2 = 0 \Rightarrow s_{1,2} = \boxed{-1 \pm j1}$$

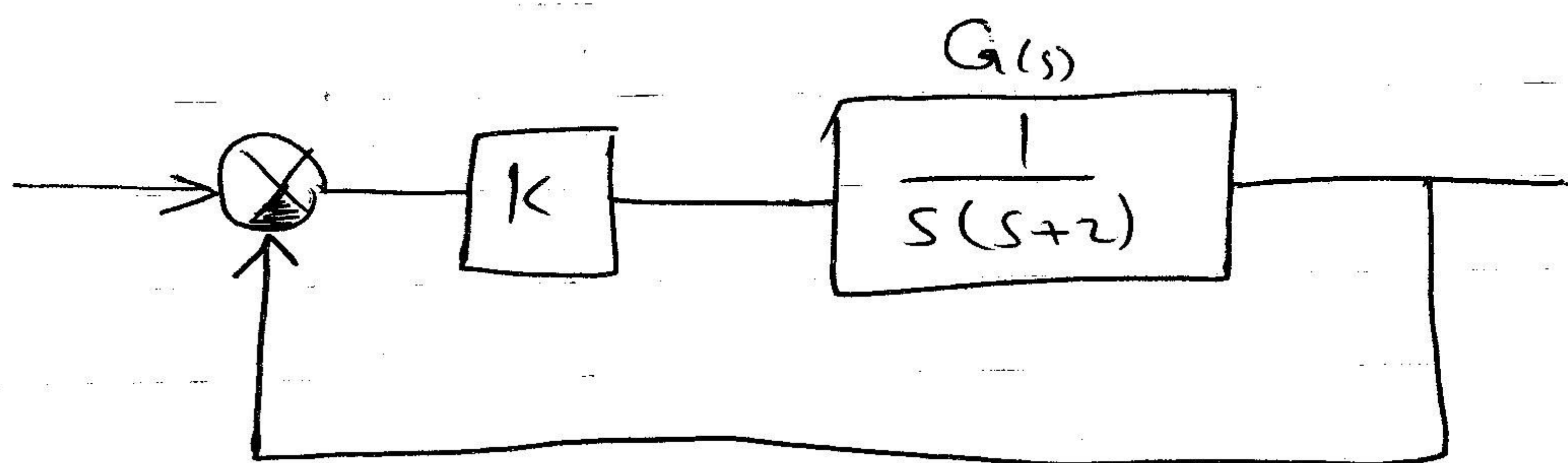
$$\textcircled{5} \quad k=4 \Rightarrow q(s) = s^2 + 2s + 4 = 0 \Rightarrow s_{1,2} = \boxed{-1 \pm j\sqrt{3}}$$

$$\textcircled{6} \quad k=\infty \Rightarrow q(s) = s^2 + 2s + \infty = 0 \Rightarrow s_{1,2} = \frac{-2 \pm \sqrt{4-\infty}}{2} = \boxed{-1 \pm j\infty}$$



12/12 2021

Back to previous example :-



$$T(s) = \frac{\frac{k}{s(s+2)}}{\frac{k}{s(s+2)} + 1}$$

$$KG(s) + 1 = 0$$

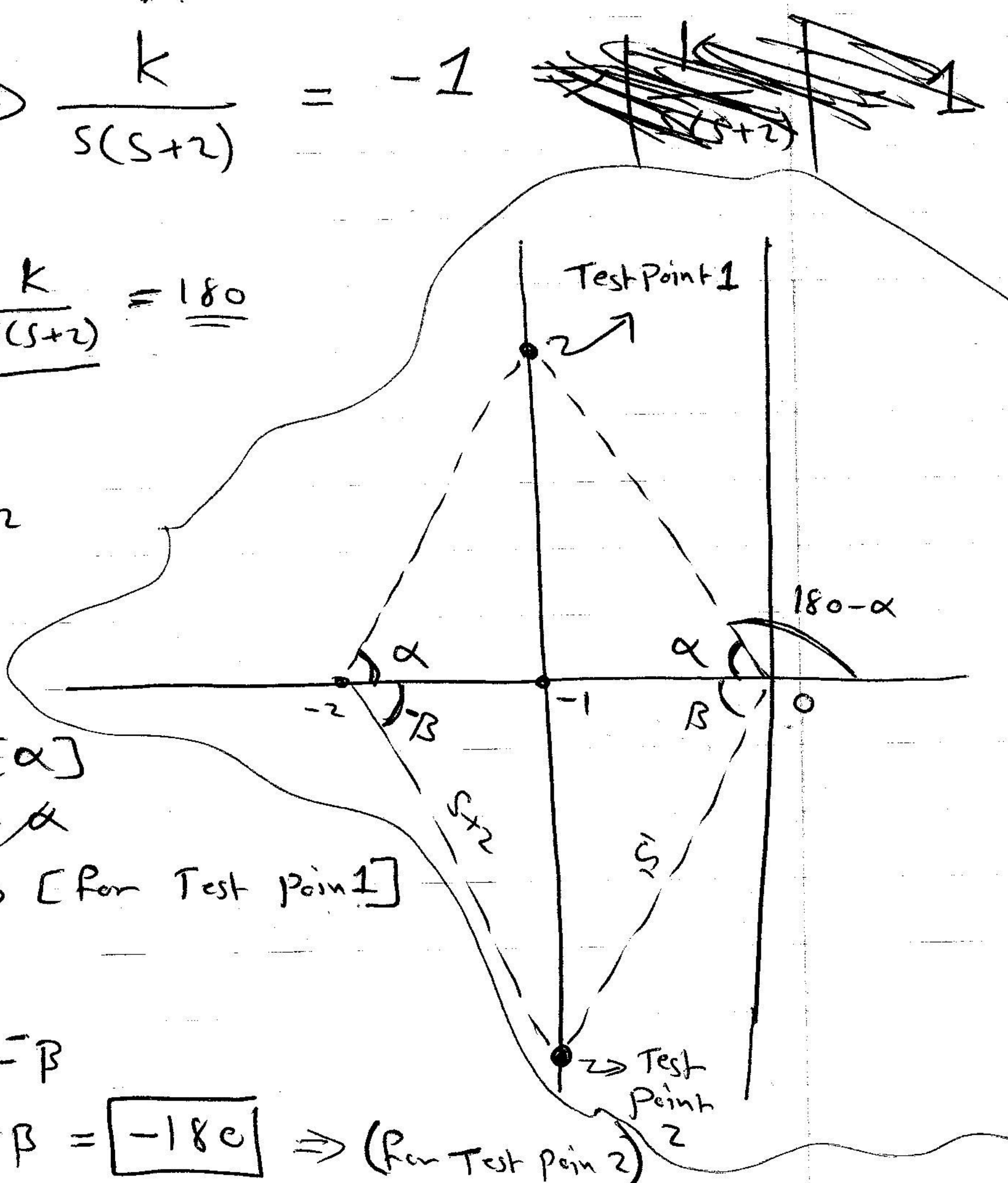
$$\frac{k}{s(s+2)} + 1 = 0 \Rightarrow \frac{k}{s(s+2)} = -1$$

$$\Rightarrow \left| \frac{k}{s(s+2)} \right| = 1 \quad \angle \frac{k}{s(s+2)} = \underline{180}$$

$$\boxed{180} = 0 - \angle s - \angle s+2$$

$$\begin{aligned} \text{angle} &= 0 - [180 - \alpha] - [\alpha] \\ &= 0 - 180 + \alpha - \alpha \\ &= \boxed{-180} \Rightarrow [\text{For Test point 1}] \end{aligned}$$

$$\begin{aligned} \text{angle} &= 0 - [180 + \beta] - \beta \\ &= -180 - \beta + \beta = \boxed{-180} \Rightarrow (\text{For Test point 2}) \end{aligned}$$



$$\left| \frac{k}{s(s+2)} \right| = 1 \Rightarrow \frac{|k|}{|s| |s+2|} = 1 \Rightarrow \frac{k}{|s| |s+2|} = 1$$

① at $k=1$ (Test Point 1) (TP1)

$$\Rightarrow \frac{1}{|1| |1|} = \boxed{1}$$

② at TP2 $k=2$

$$\frac{k}{|s| |s+2|} = 1$$

$$|s| = \sqrt{1^2 + 1^2} = \sqrt{2}$$

$$|s+2| = \sqrt{1^2 + 1^2} = \sqrt{2}$$

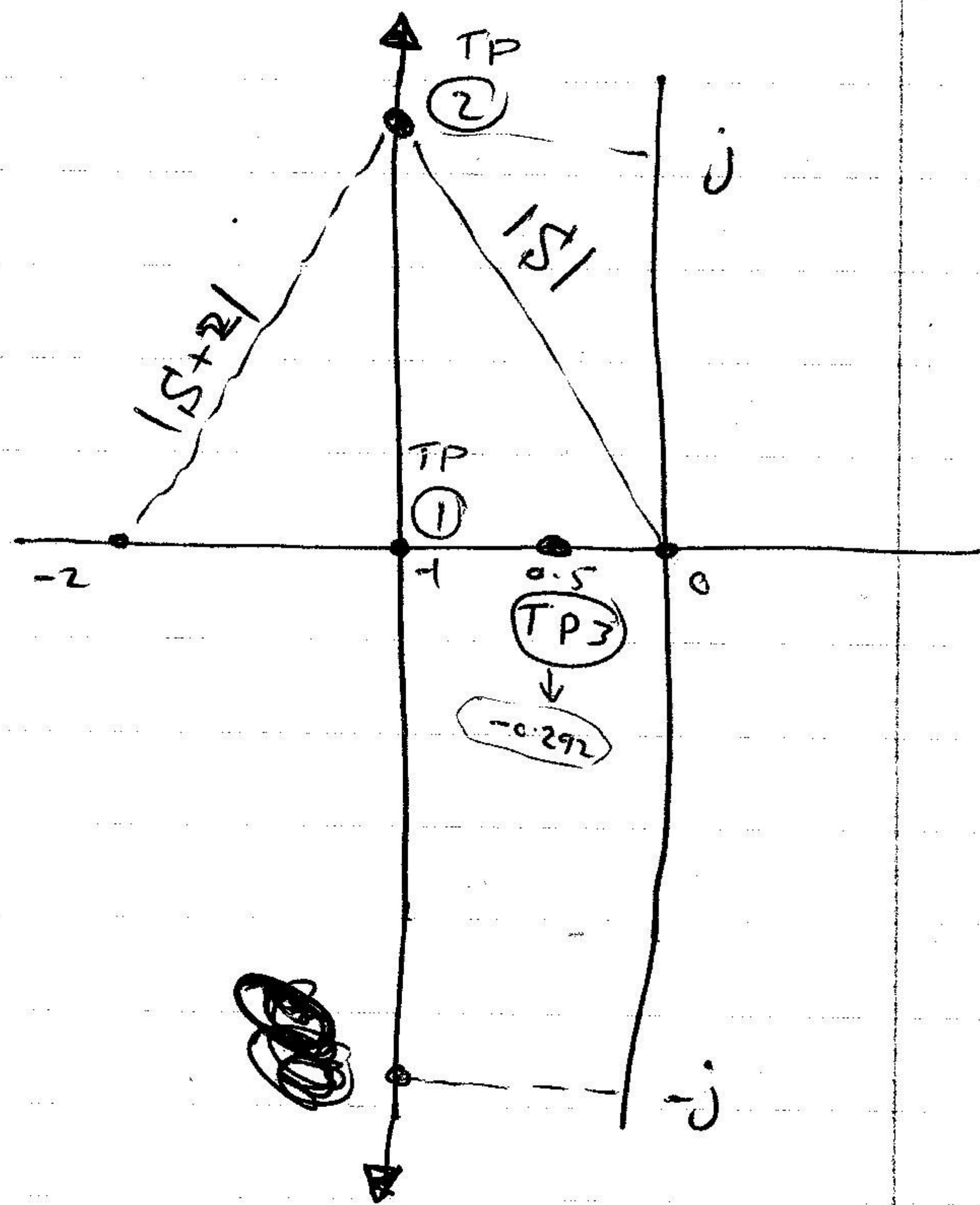
$$\Rightarrow \frac{k}{\sqrt{2} * \sqrt{2}} = \frac{2}{\sqrt{2} \sqrt{2}} = \frac{2}{2} = \boxed{1}$$

③ at TP3 at $k=0.5$

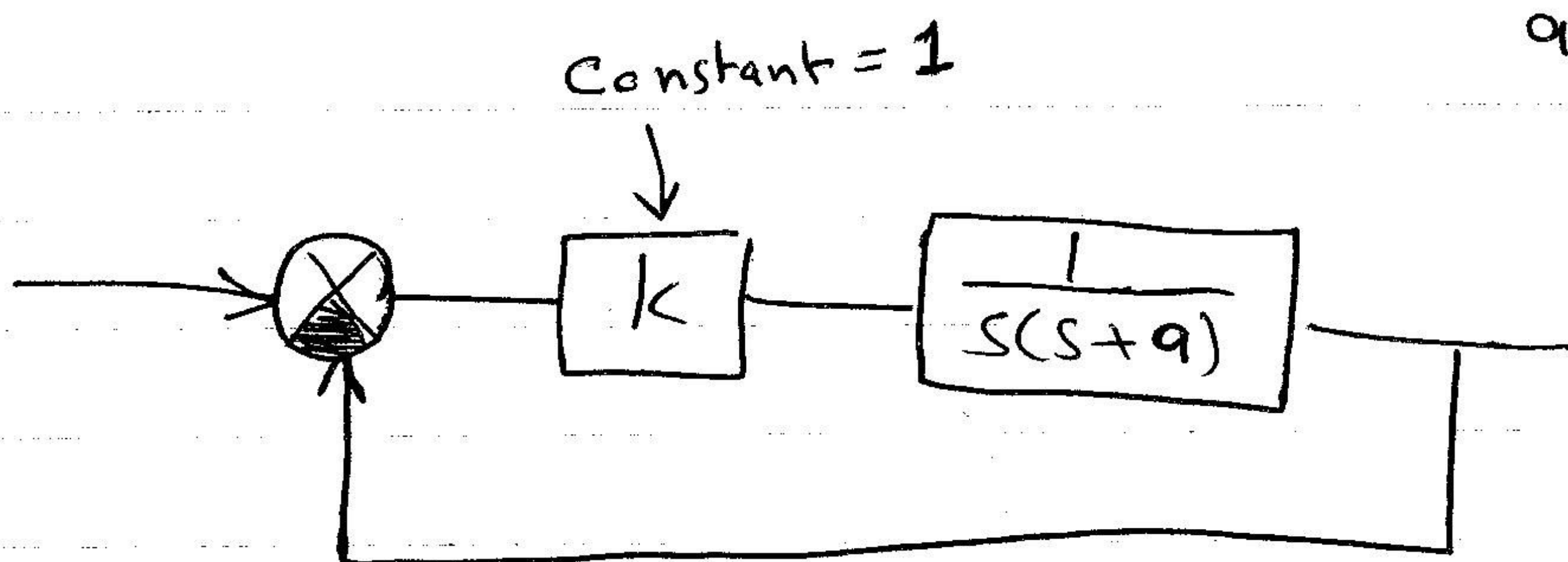
$$|s| = \boxed{0.292}$$

$$|s+2| = \boxed{1.708}$$

$$\Rightarrow \frac{k}{|s| |s+2|} = \frac{0.5}{|0.292| |1.708|} = 1.0025 \approx \boxed{1}$$



EX



k is constant
 a is Variable

$$KG(s) = -1$$

$$|KG(s)| = 1$$

$$\angle KG(s) = -180^\circ$$

but a is the Variable

$$aG(s) = -1$$

$$\angle aG(s) = -180^\circ$$

$$\Rightarrow \frac{-\frac{1}{s(s+a)}}{1 + \frac{1}{s(s+a)}}$$

$$\Rightarrow \frac{1}{s(s+a)} + 1 = 0$$

$$1 + s^2 + sa = 0$$

$$as + s^2 + 1 = 0 \quad \div s^2 + 1$$

$$a \frac{s}{s^2 + 1} + 1 = 0$$

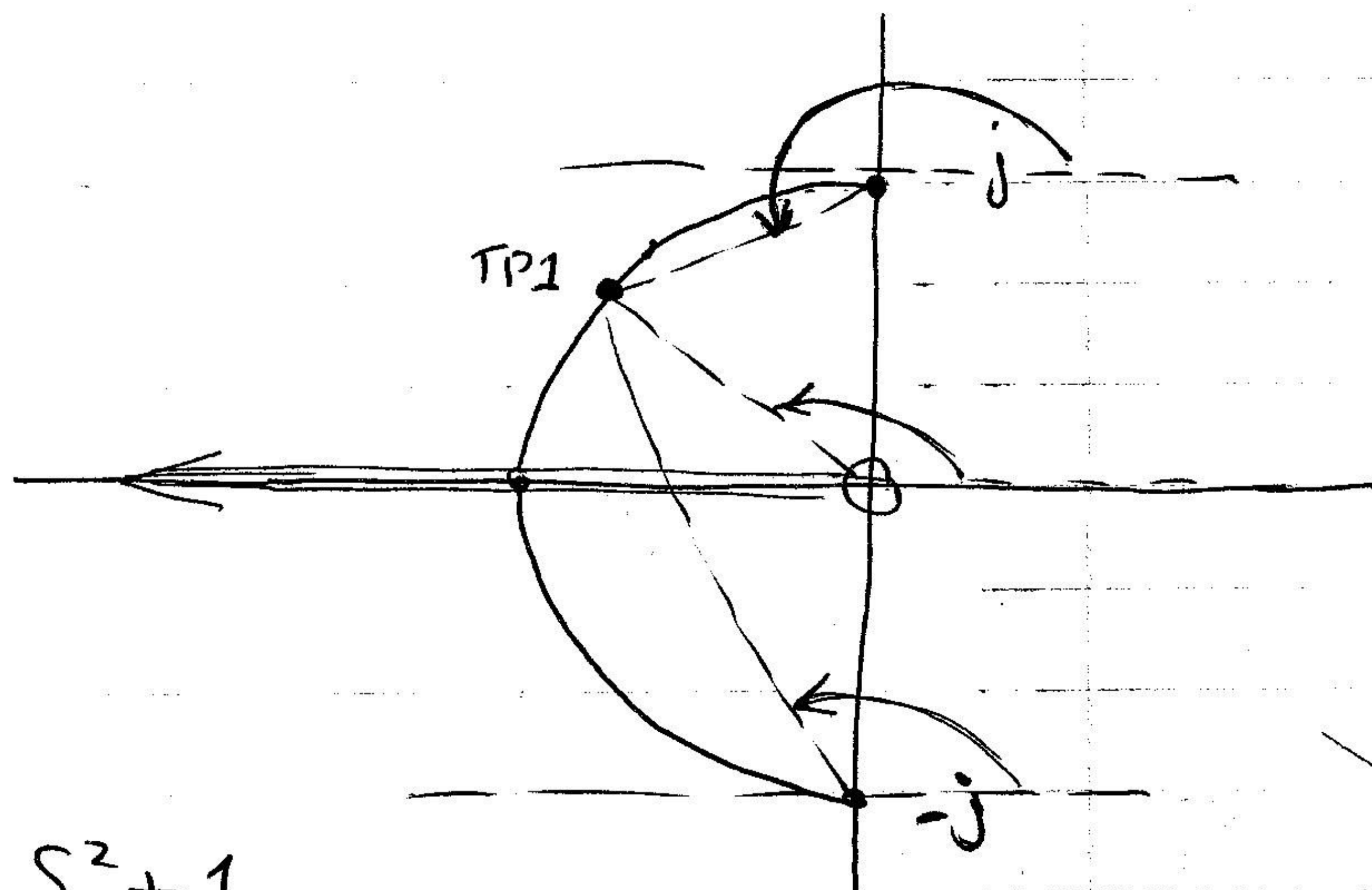
$$\Rightarrow a \frac{s}{s^2 + 1} + 1 = 0$$

$$\left| \frac{as}{s^2 + 1} \right| = 1 \Rightarrow$$

$$\frac{a |s|}{|s+j| |s-j|}$$

$$\angle \frac{as}{s^2 + 1} = -180^\circ$$

$$\Rightarrow -180^\circ = |s| - |s+j| - |s-j|$$



Root Locus Procedures

★ **STEP 1** Write the characteristic equation as

$$1 + F(s) = 0$$

Then arrange the equation so that the parameter of interest appears as the multiplying factor $1 + K P(s) = 0$

note: in most cases, $F(s) \neq K P(s)$

$$1 + \frac{s}{s+a} = 0 \quad \xrightarrow{F(s)}$$

$$s + a + s = 0$$

$$2s + a = 0 \quad / 2s$$

$$1 + \frac{a}{2s} = 0$$

$$1 + a P(s)$$

STEP 2 Write the polynomial in the form of Poles & Zeros

$$1 + K \frac{\prod_{i=1}^m (s + z_i)}{\prod_{j=1}^n (s + p_j)}$$

STEP 3 Locate the poles & Zeros on the s-Plane with Selected Symbols as K varies from $0 \rightarrow \infty$

pole	X
Zero	O

المعادلة = $\frac{1}{s}$

Ex Rewrite the equation in the following form :-

$$\prod_{i=1}^n (s + p_i) + K \prod_{i=1}^m (s + z_i)$$

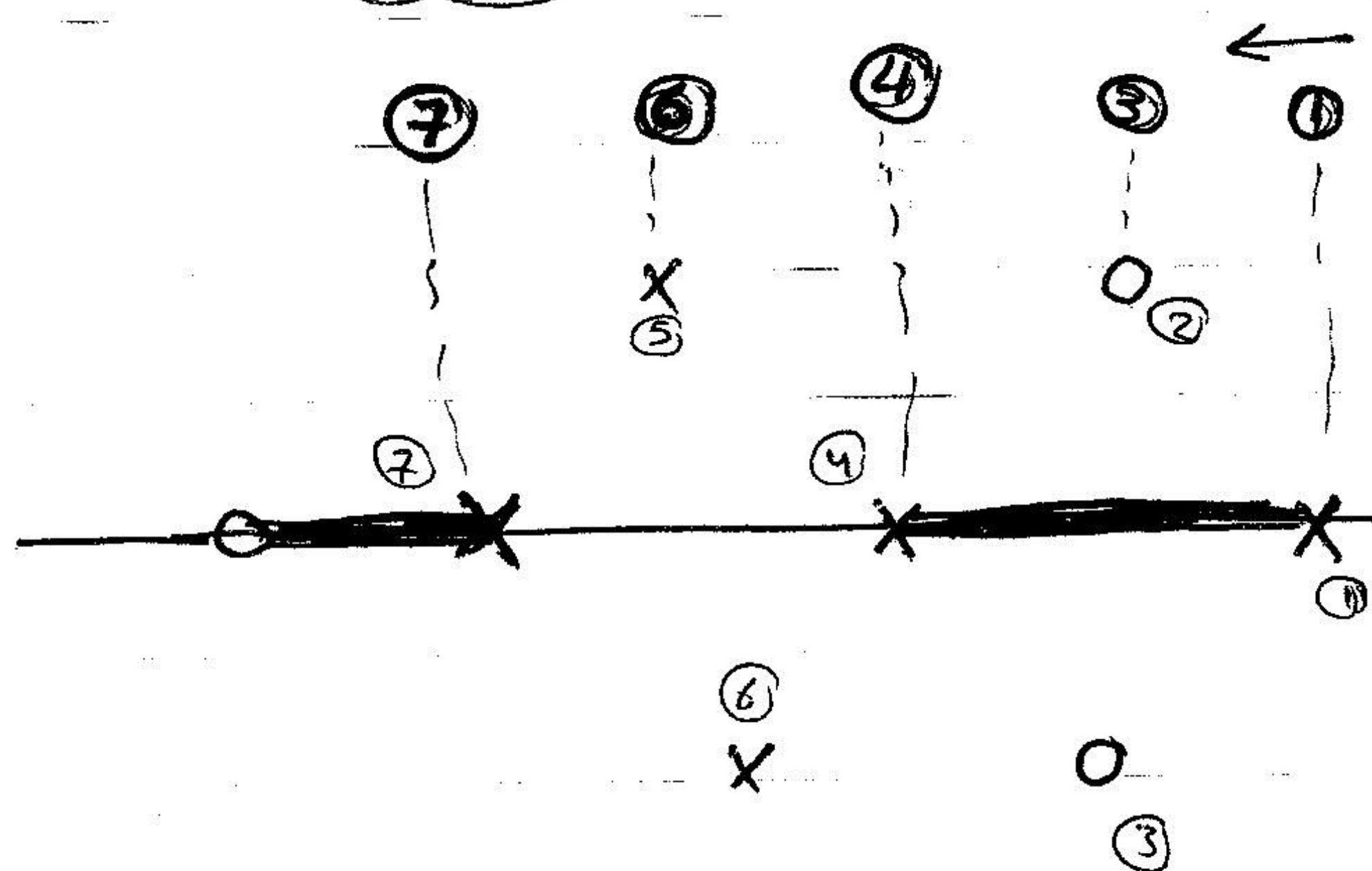
When $K=0 \Rightarrow$ The roots of ch. equ. are simply the poles of $P(s)$.

When $K=\infty \Rightarrow$ The roots of ch. equ. are simply the zeros of $P(s)$.

* There is $n-m$ branches of the root Locus approaches ∞

STEP 4 Locate the segment of the real-axis that are root Loci

"The root Locus on the real-axis always lies in a section of the real-axis to the left of an odd number of poles & zeros"



مبدأ اختيار المسار (يُجب أن يجمع الـ Poles)

دار Zeros (إذا وجدنا العدد فردي)

يكون هناك رسم Root locus عبه

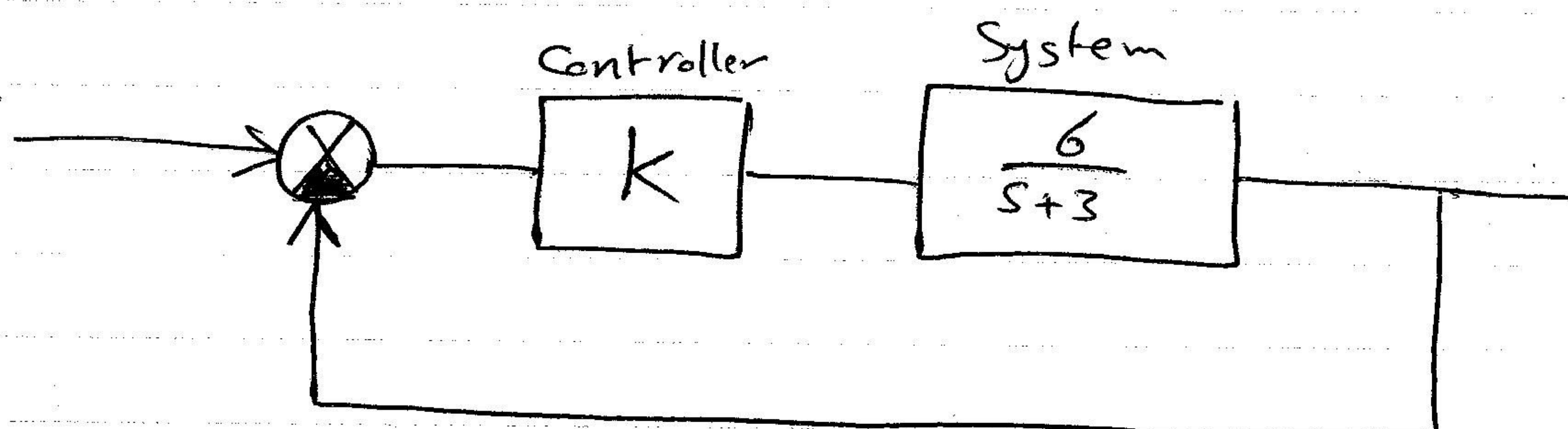
نفضل مسير في المسار

من اليمين إلى اليسار

إذا أصبح مجموع الأقطاب والاصناف زوجي

لا يكون هناك رسم عبه، وهكذا

Example :- plot the root Locus of the following system as k varies from zero to ∞ .



$$T(s) = \frac{\frac{6k}{s+3}}{1 + \frac{6k}{s+3}}$$

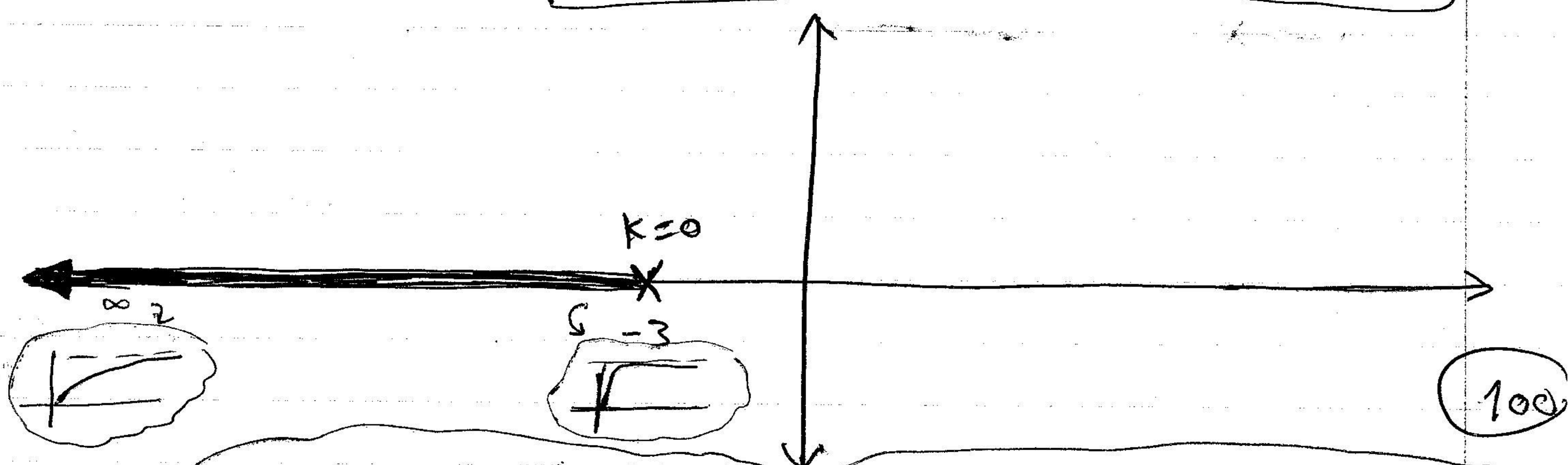
STEP 1 $1 + \frac{6k}{s+3} = 0 \equiv 1 + F(s) = 0$

STEP 2 $1 + K \frac{6}{s+3} = 0$ ← حاسة هنا
مدقة زبط

STEP 3 $1 + K \frac{6}{(s+3)}$

STEP 4 Poles $\Rightarrow S = -3$

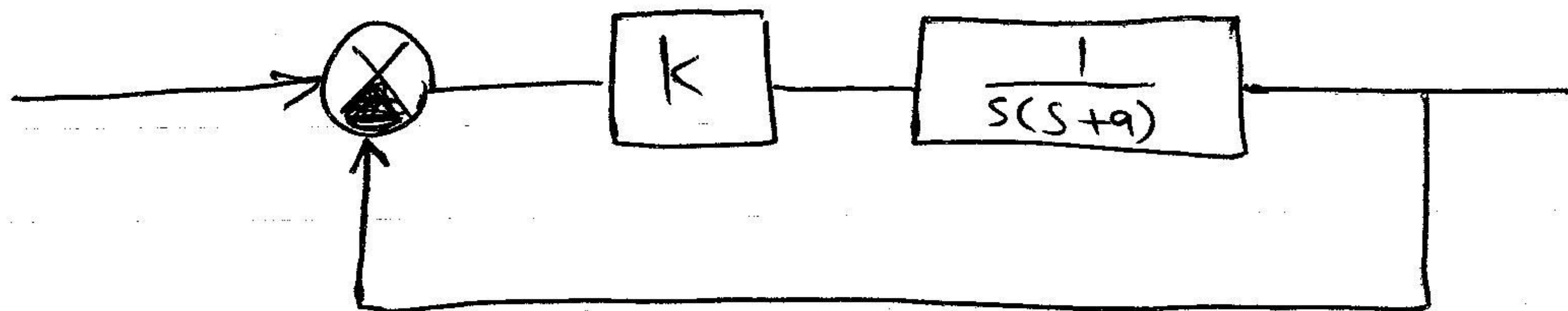
Zeros \Rightarrow Not available, but there is one goes to ∞



ملاحظة :- إذا كان نظام من الدرجة الأولى، فالخطوات الأربعة الأولى كافية لرسم Root Locus.

Ex :-

as $a = 0 \rightarrow \infty$



$$T(s) = \frac{\frac{k}{s(s+a)}}{1 + \frac{k}{s(s+a)}}$$

STEP 1 : $1 + F(s) = 0$

$$1 + \frac{k}{s(s+a)} = 0$$

STEP 2 : $1 + \frac{k}{s(s+a)} = 0$

$$1 + a p(s) = 0$$

$$s(s+a) + k = 0$$

$$s^2 + as + k = 0$$

$$s^2 + k + as = 0 \quad \div (s^2 + k)$$

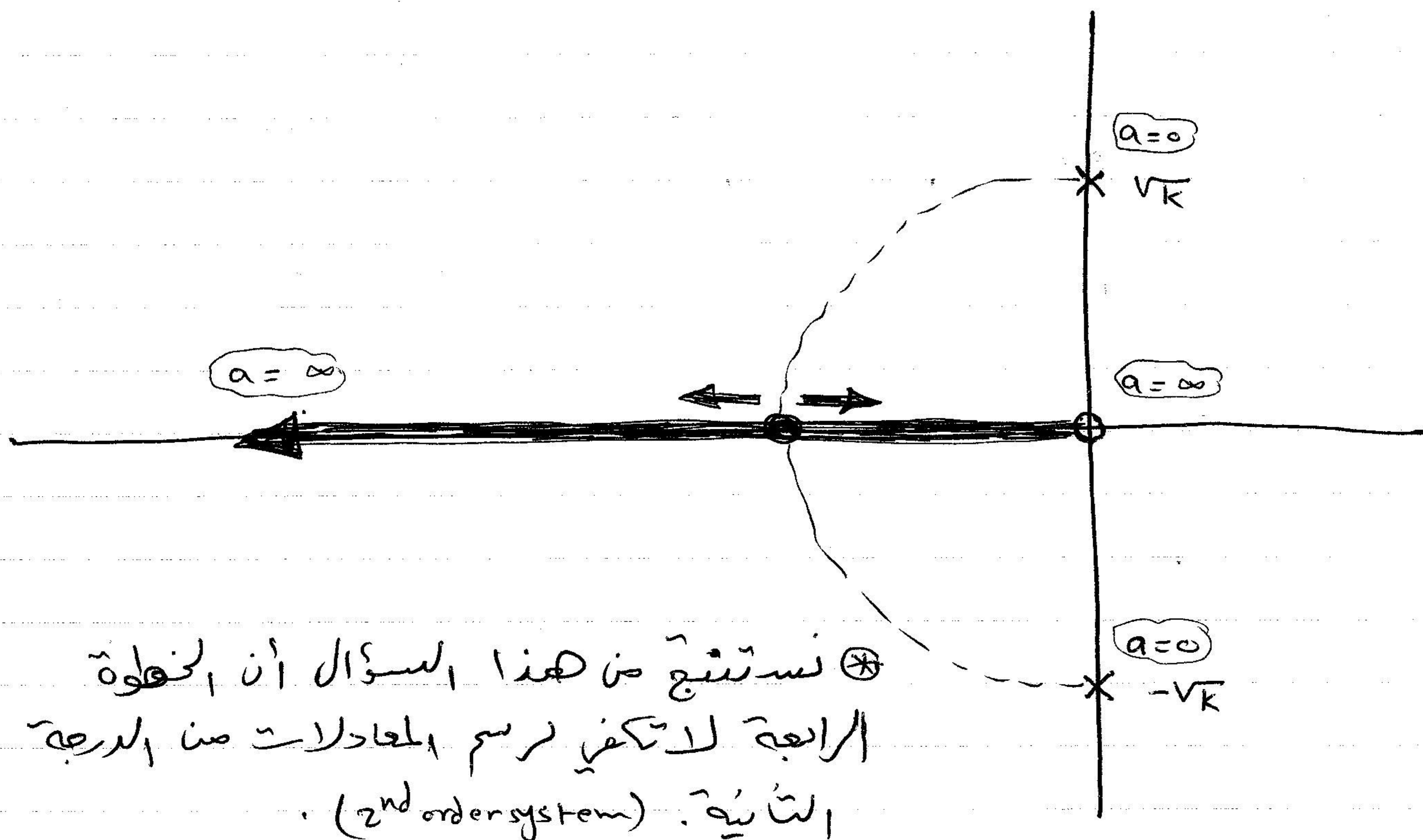
$$\Rightarrow \left[1 + \frac{as}{s^2 + k} \right] \rightarrow 1 + a p(s) = 0$$

أصبحت على صورة القياسية

STEP 3 : $1 + a \frac{s}{s^2 + k} = 0 \Rightarrow 1 + a \frac{s}{(s+j\sqrt{k})(s-j\sqrt{k})} = 0$

STEP 4 :- Poles : $s = \pm j\sqrt{k}$
Zeros : $s = 0$

Pole conjugate always symmetrical



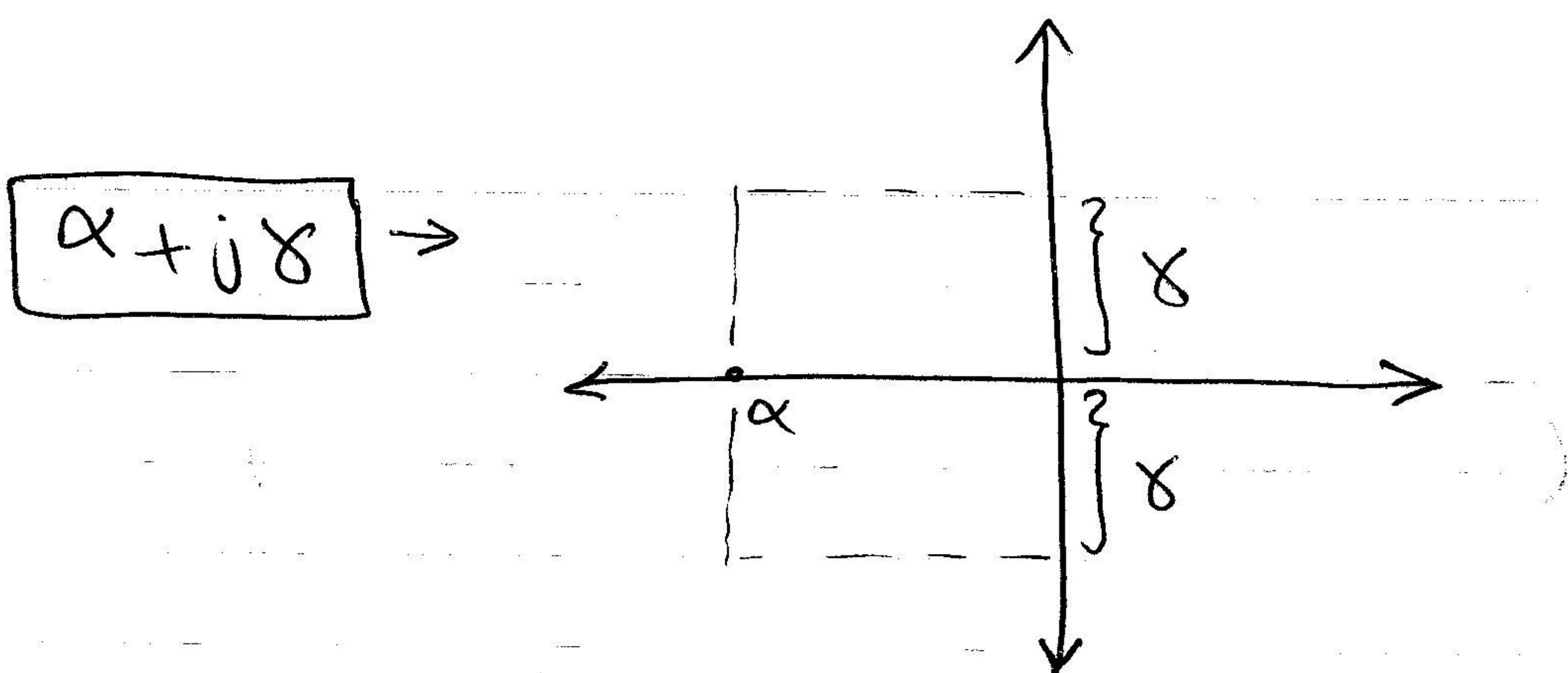
Back To General STEPS - [عودة الخطوات الرئيسية]

STEP 5 Determine the number of separate loci

$$\text{No of Separate Loci} = \text{No of Poles}$$

STEP 6 The root Loci must be symmetrical with respect to the horizontal real-axis, because the complex roots must appear as pole conjugate.

$$S_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a} = \frac{-b}{2a} \pm \frac{j9}{2a} = \alpha \pm j\gamma$$



STEP 7 The Loci proceeds to the zero at ∞ along asymptote centered at σ_A , and with angle ϕ_A , when the N_0 of ~~poles of $P(s)$~~ finite zeros of $P(s)$ is less than the N_0 of poles of $P(s)$

$N_z < N_p$ Then we have N_0 of zeros at ∞

$$N = N_p - N_z$$

These Linear asymptotes are centered at a point on the real axis & given by :-

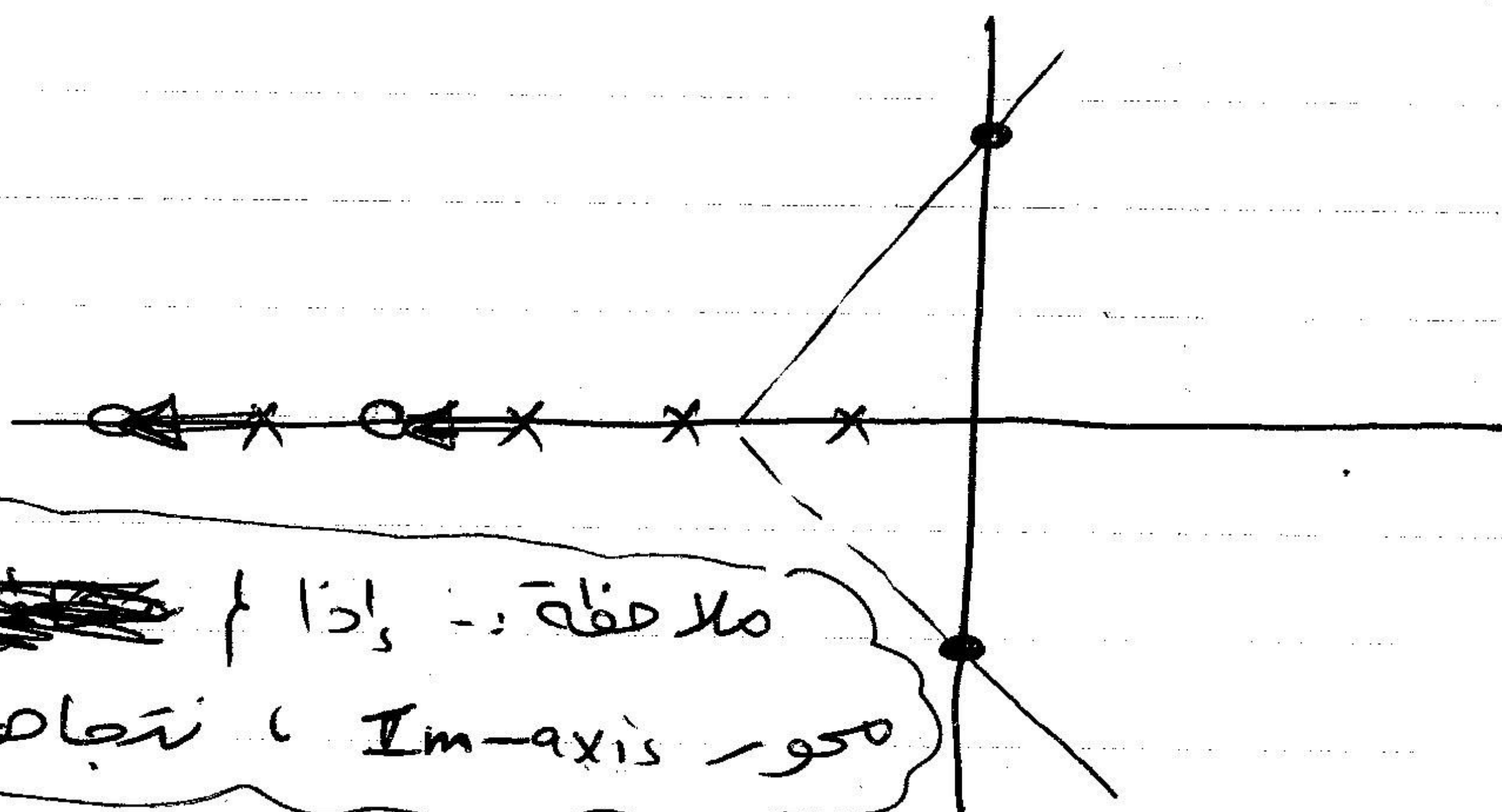
$$\sigma_A = \frac{\sum \text{Poles of } P(s) - \sum \text{Zeros of } P(s)}{N_p - N_z}$$

* The angle of asymptotes with respect to real axis is given by :-

$$\phi_A = \frac{2q + 1}{N_p - N_z} \times 180 \quad q = (0, 1, 2, 3 \dots N_p - N_z - 1)$$

STEP 8

Determine the point of which the root Locus Crosses the Imaginary-axis (Use Routh Hurwitz Criteria)

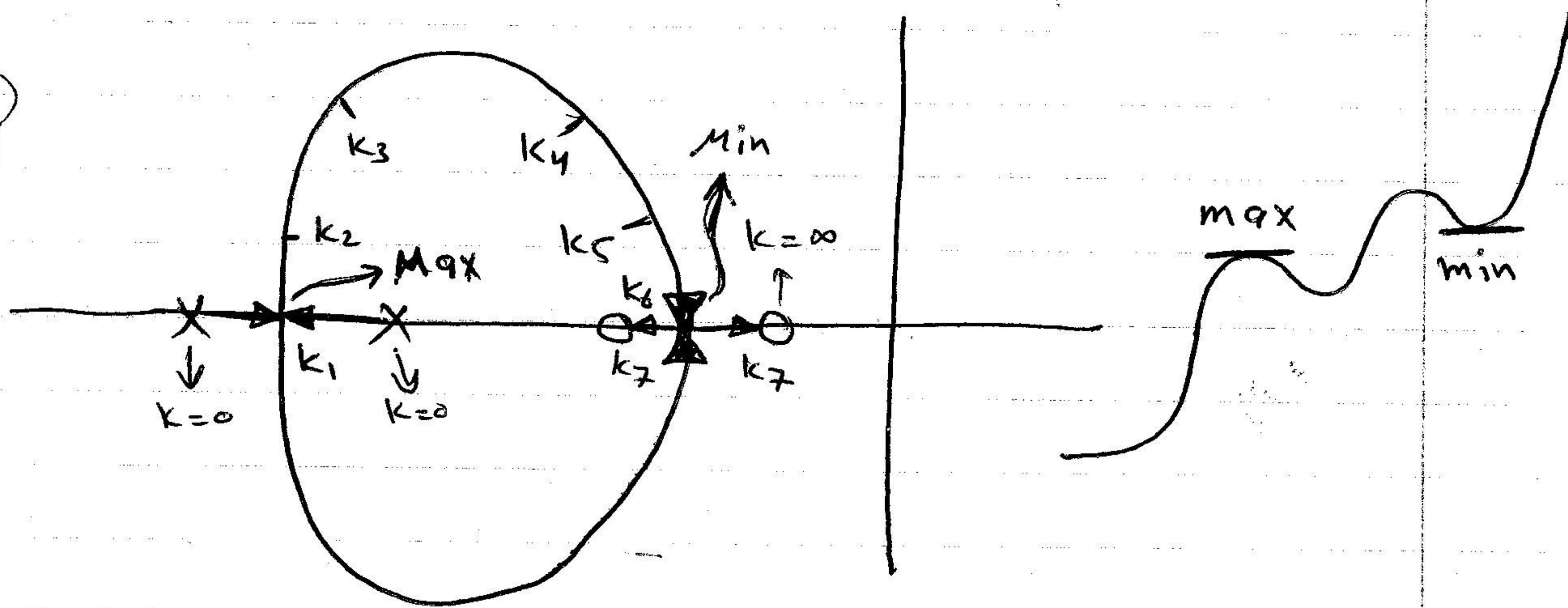


ملاحظة :- إذا لم يكن هناك تقاطع مع $Im\text{-axis}$ ، نتجاهل الخطوة ١٠.

STEP 9

Determine the Break-away & Break-in points.

X : pole
O : zero



① Put or Find the equation of k

$$1 + kP(s) = 0 \Rightarrow k = \frac{-1}{P(s)}$$

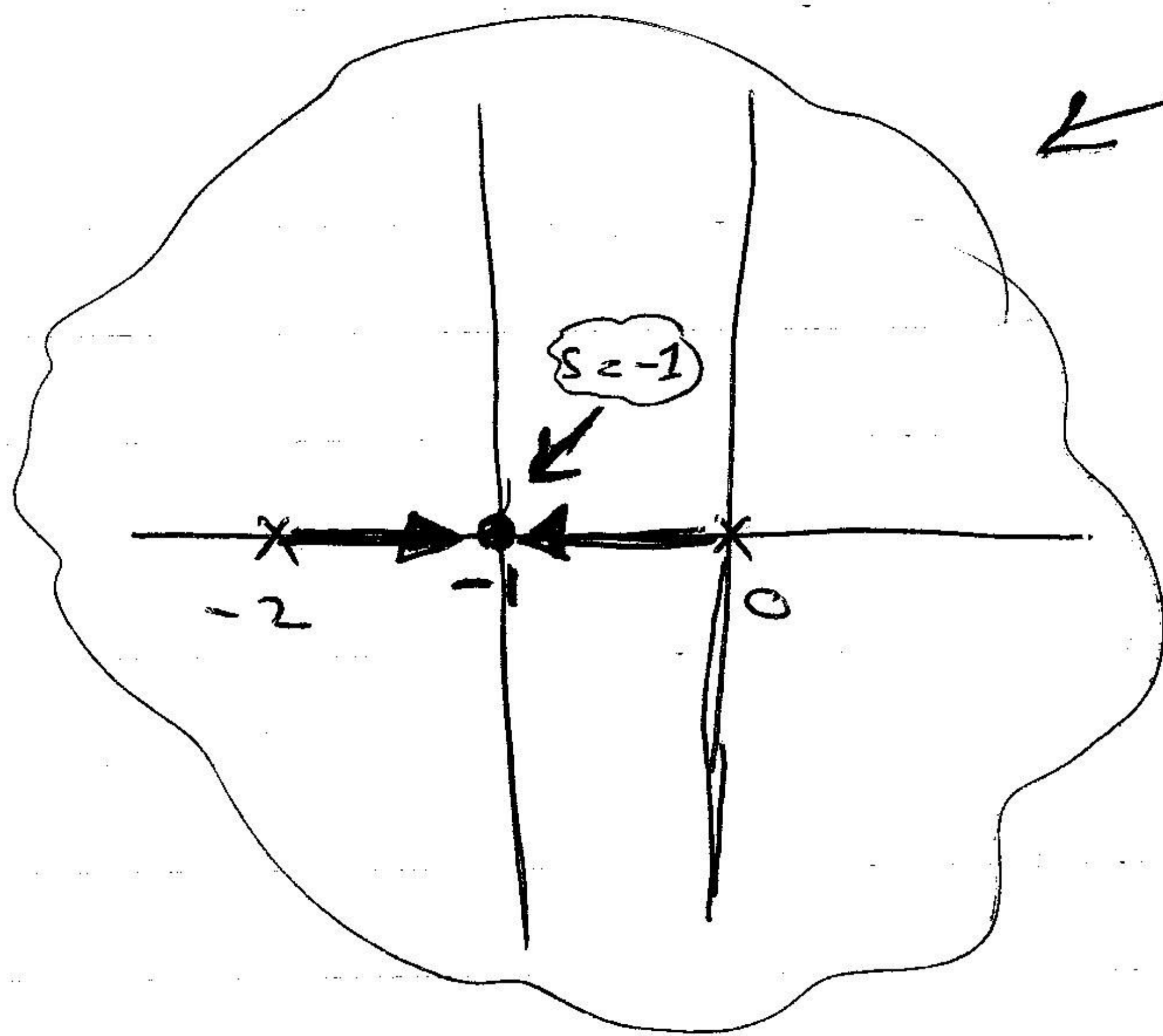
② Find $\frac{dk}{ds} = 0$

Ex $1 + \frac{k}{s(s+2)} = 0$

$$k = -s(s+2)$$

$$k = -s^2 - 2s$$

$$\frac{dk}{ds} = -2s - 2 = 0 \Rightarrow -2s = 2 \Rightarrow \boxed{s = -1}$$

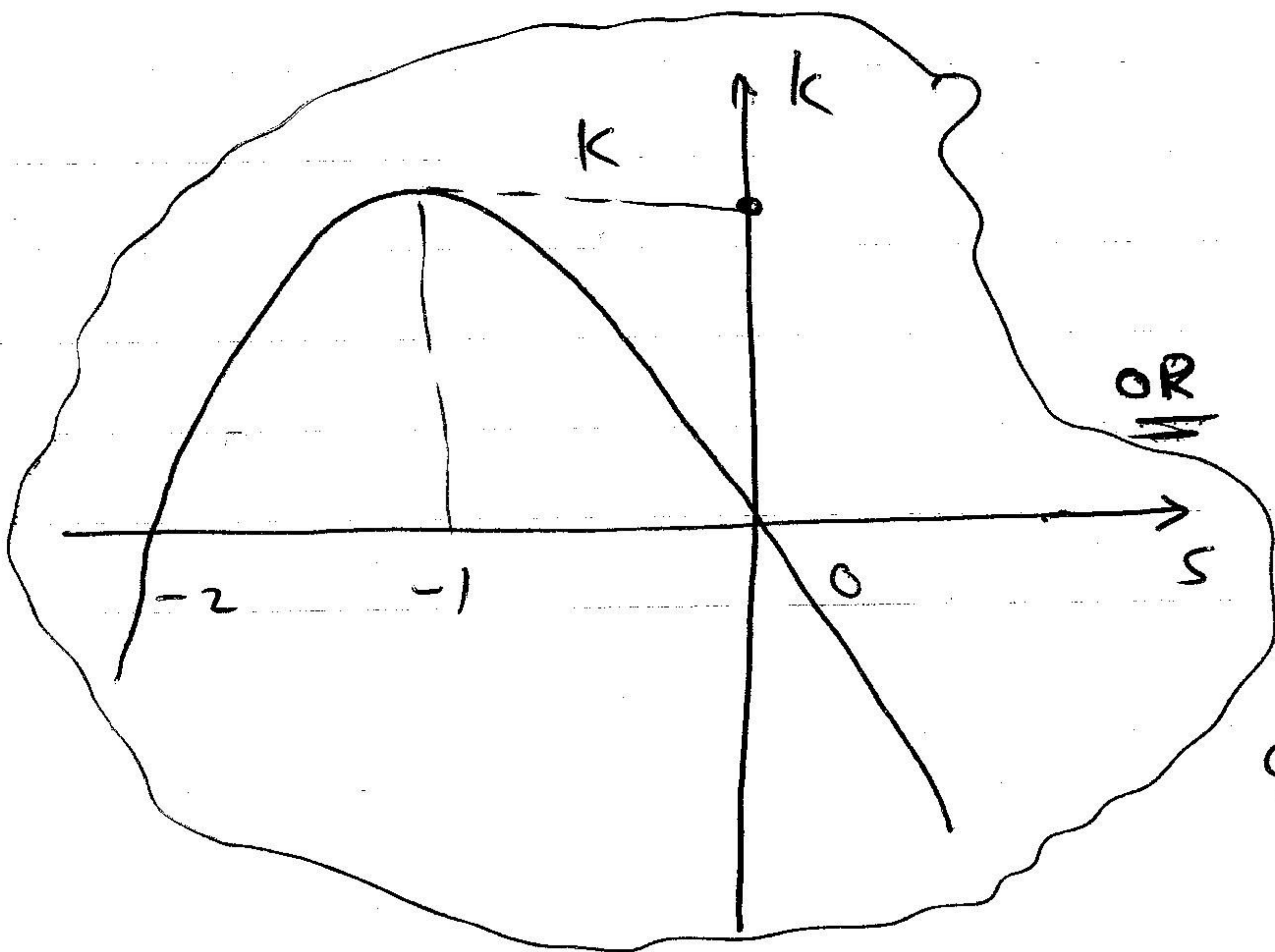


طرق حل الخطوة التاسعة

① ايجاد المشتقة $\frac{dk}{ds} = 0$

② إعطاء Table للـ k قيم min و max الخاصة بـ k

③ إعطاء صحن للـ k قيم min و max الخاصة بـ k



OR

s	0	-1	-2	-3
k	0	1	0.2	0.1

OR

$$\frac{dk}{ds} = 0$$

Ex Find the root Locus of the following system

$$1 + \frac{K}{(s+2)(s+4)} = 0$$

- **STEP 1** already done.

- **STEP 2** already done.

STEP 3 Poles: $s = -2$ $s = -4$

STEP 4 determine the Loci Segment.

STEP 5 No of Loci = 2.

STEP 6 will be taken in consideration.

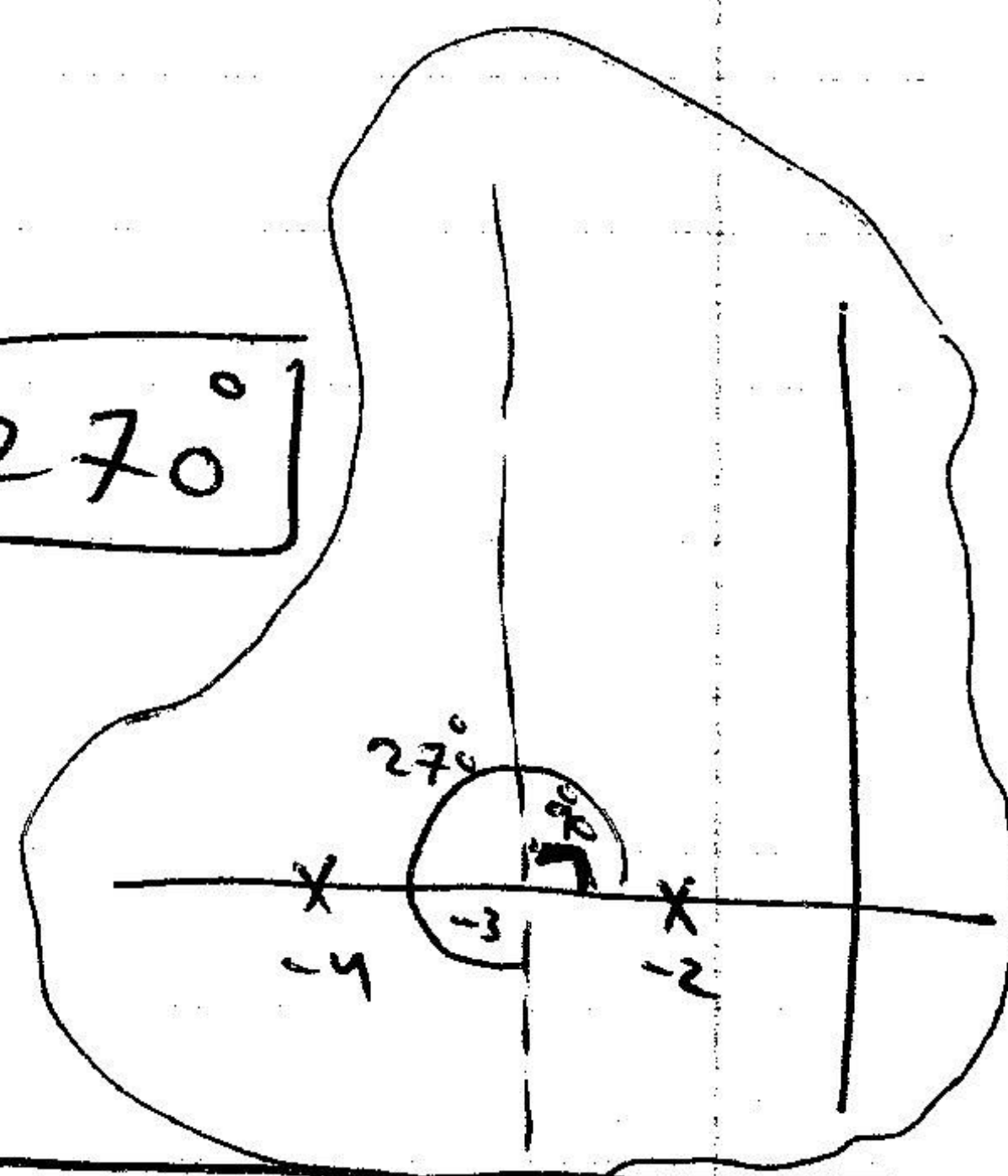
$$\begin{aligned} \text{STEP 7 } \phi_A &= \frac{\sum \text{Poles} - \sum \text{Zeros}}{N_P - N_Z} = \frac{-2 - 4 - (0)}{2 - 0} \\ &= \frac{-6}{2} = \boxed{-3} \end{aligned}$$

$$\phi_A = \frac{2q+1}{2} * 180 \quad ; \quad q = 0, 1$$

$$\phi_A = \frac{2(0)+1}{2} * 180 = \frac{1}{2} * 180 = \boxed{90^\circ}$$

$$\phi_A = \frac{2(1)+1}{2} * 180 = \frac{3}{2} * 180 = \boxed{270^\circ}$$

$$\therefore \phi_A = 90^\circ, 270^\circ$$



STEP 8 No intersect with Imaginary axis

STEP 9 $K = -(s+2)(s+4)$

$$K = -s^2 - 6s - 8$$

$$\frac{dK}{ds} = -2s - 6 = 0 \Rightarrow -2s = 6 \Rightarrow \boxed{s = -3}$$

صوتة كانت نقطة Breakway ~~Breakway~~ من نفسا نقطة Centroid 6A

إذا كان عندنا نقطتين مثلا
 $s = -3$
 $s = -5$

واحدة منهن ستكون Breakaway

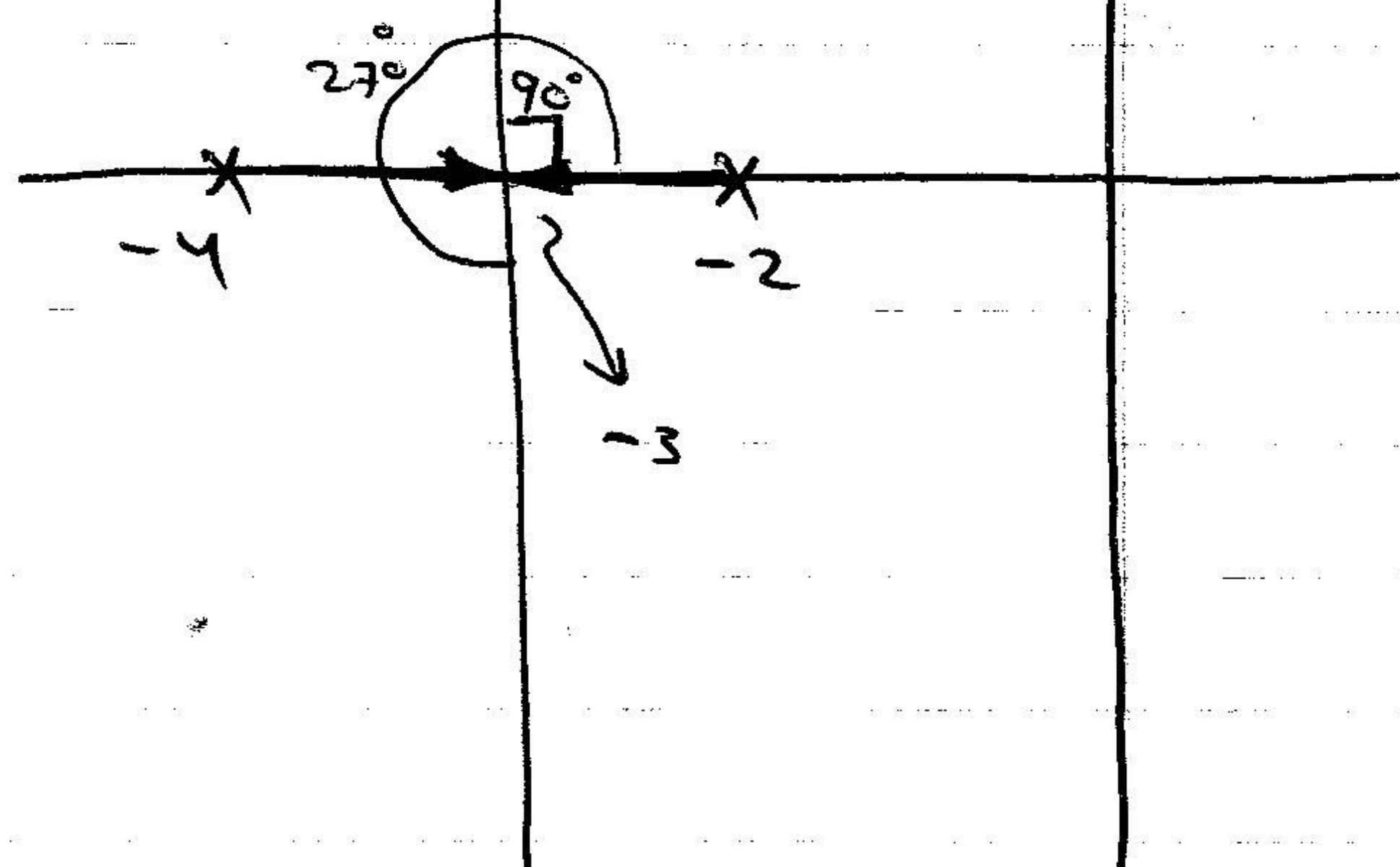
والاخرى ستكون Breakin

كيف عرف ذلك؟

نخفض قيمة s في اللاحقة

قيمة K الاربعة من Breakaway

قيمة K الاصغر من Breakin



Ex Find the root Locus of the following systems

$$1 + K \frac{(s+1)}{s(s+2)(s+4)^2} = 0$$

K	0	0.412	0.412	0.417	0.39
s	-2	-2.4	-2.45	-2.5	-2.1

STEP 1 already done

STEP 2 already done

STEP 3 Poles: $s = 0, -2, -4, -4$

Zeros: $s = -1$

STEP 4 Locating segments on real-axis

STEP 5 :- No of Separate Loci = No of poles = 4

STEP 6 To be Taken in Consideration

STEP 7 $\phi_A = \frac{\sum \text{Poles} - \sum \text{Zeros}}{N_P - N_Z} = \frac{0 - 2 - 4 - 4 - (-1)}{3} = \boxed{-3}$

$$\phi_A = \frac{2q+1}{N_P - N_Z} * 180, \quad q = 0, 1, 2$$

$$\phi_A = \frac{2q+1}{3} * 180 \Rightarrow \phi_A = \underline{60}, \underline{180}, \underline{300}$$

STEP 8 $1 + \frac{k(s+1)}{s(s+2)(s+4)^2} = 0 \Rightarrow s(s+2)(s+4)^2 + k(s+1) = 0$

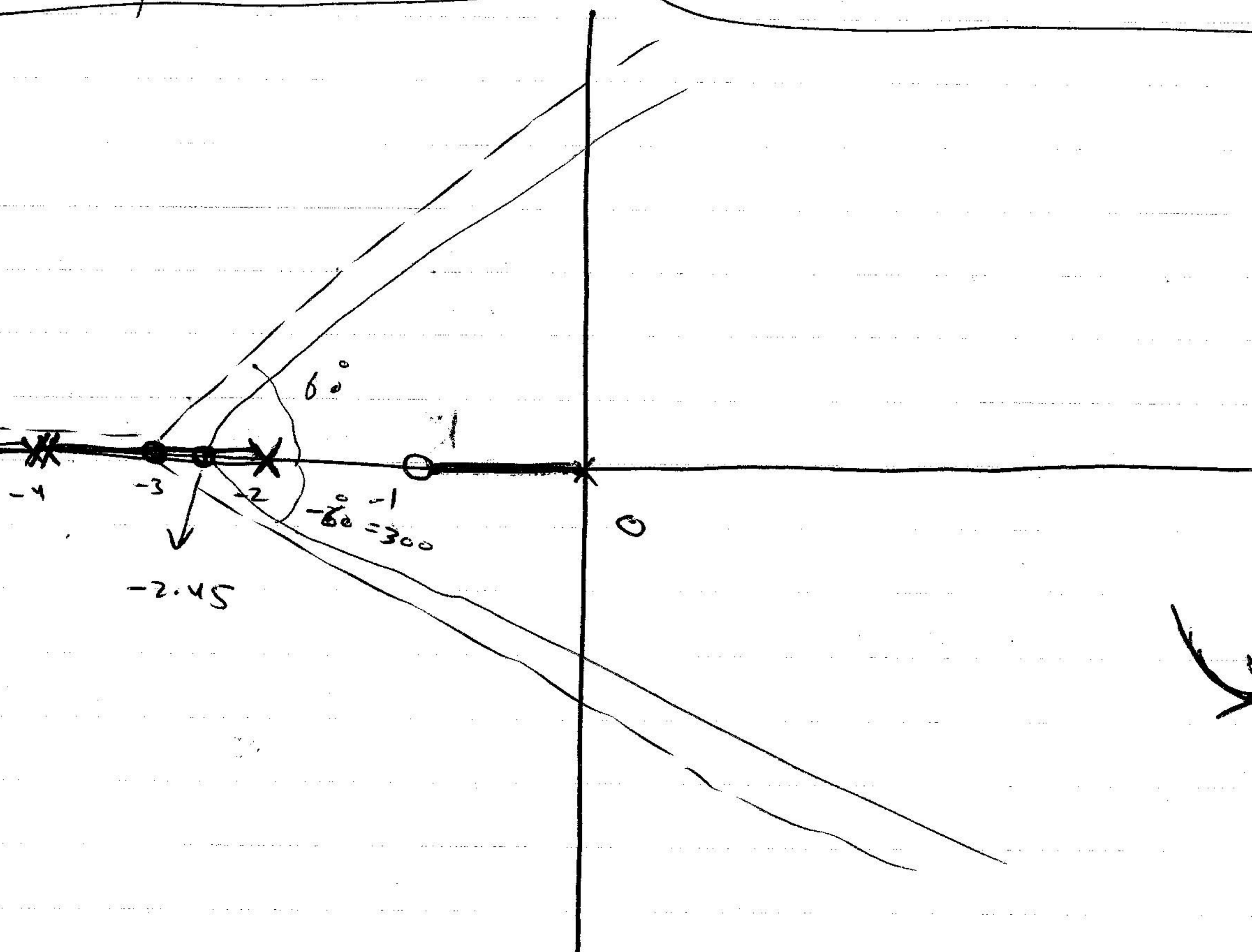
at Home

لايجاد متقاطع مع محور

s^4
 s^3
 s^2
 s^1
 1

$$\begin{array}{c|c} \hline & \\ \hline 1-k & 0 \\ \hline \end{array}$$

Take this equation and find the intersection points with Imaginary-axis



Breakaway point :-

STEP 9 $S = -2.45$


Back To General STEPS

STEP 10

Determine the angle of departure ^{بالفأرة} \angle ~~the~~ the angle of arrival ^{الوصول} Using the phase angle criteria.

$$\phi = \pm 180 (2q + 1)$$

Take $\phi = \pm 180$ at $q = 0$
180

Example $G H(s) = \frac{k}{(s+p_3)(s^2 + 2\zeta\omega_n s + \omega_n^2)}$ 

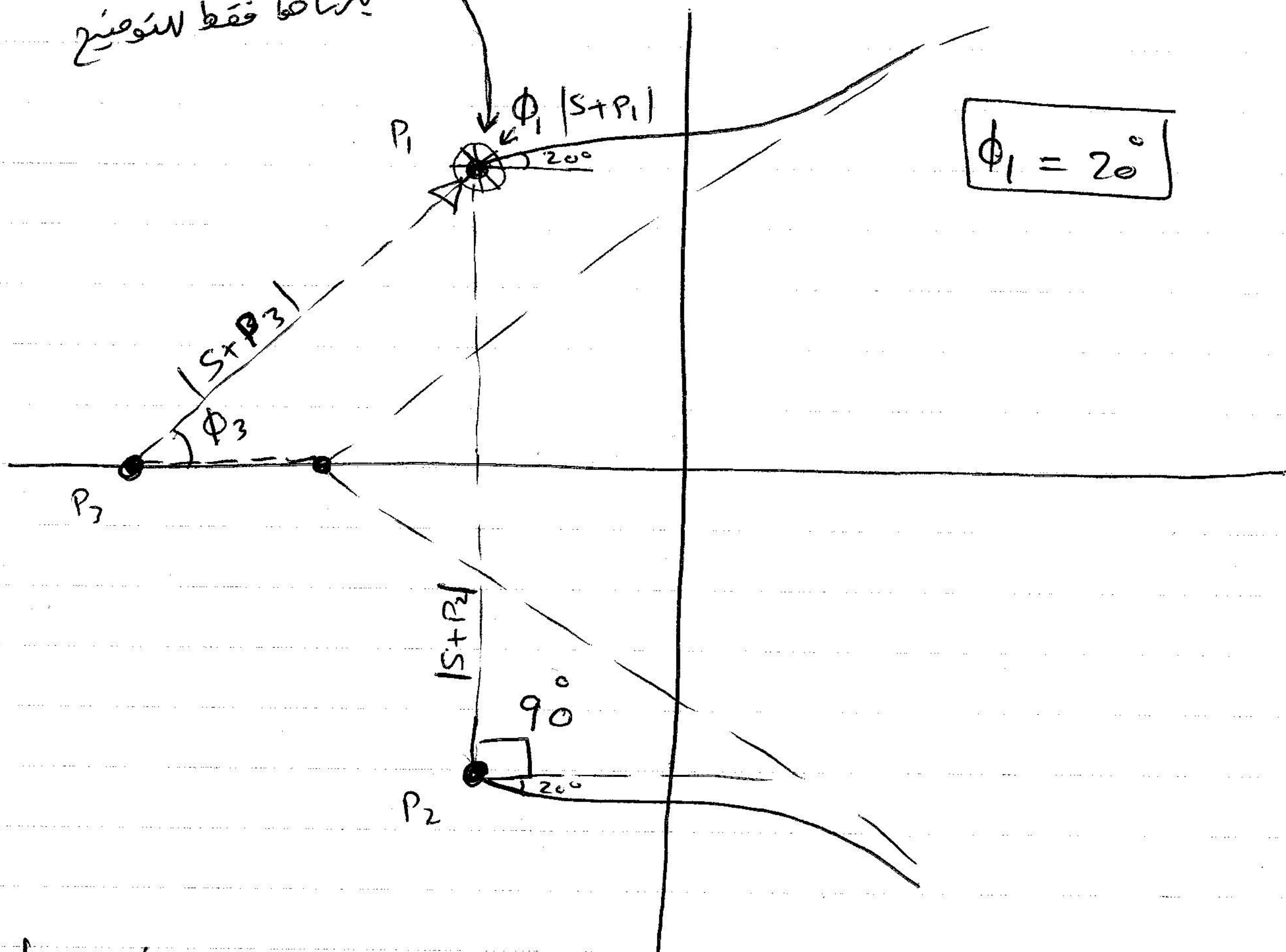
$$= \frac{k}{(s+p_3) \underbrace{(s+p_1)(s+p_2)}_{\text{Pole Conjugate}}}$$

$$\phi_A = \frac{p_1 + p_2 + p_3}{3 - 0}$$

$$\phi_A = \frac{(2q+1)}{3} * 180 \quad (q = 0, 1, 2)$$

$\phi = 60, 180, 300$

من عبارة عند دائرة نصف قطرها صفر
ليتنا فقط للتوضيح



$$\phi_1 + \phi_2 + \phi_3 = 180$$

$$\phi_1 + 90 + \phi_3 = 180$$

$$\phi_1 = 90 - \phi_3$$

Suppose that $\phi_3 = 70^\circ$ مجرد افتراض

$$\therefore \phi_1 = 90 - 70 = 20^\circ$$

angle of departure :



زاوية الانحدار
for poles

angle of arrival :



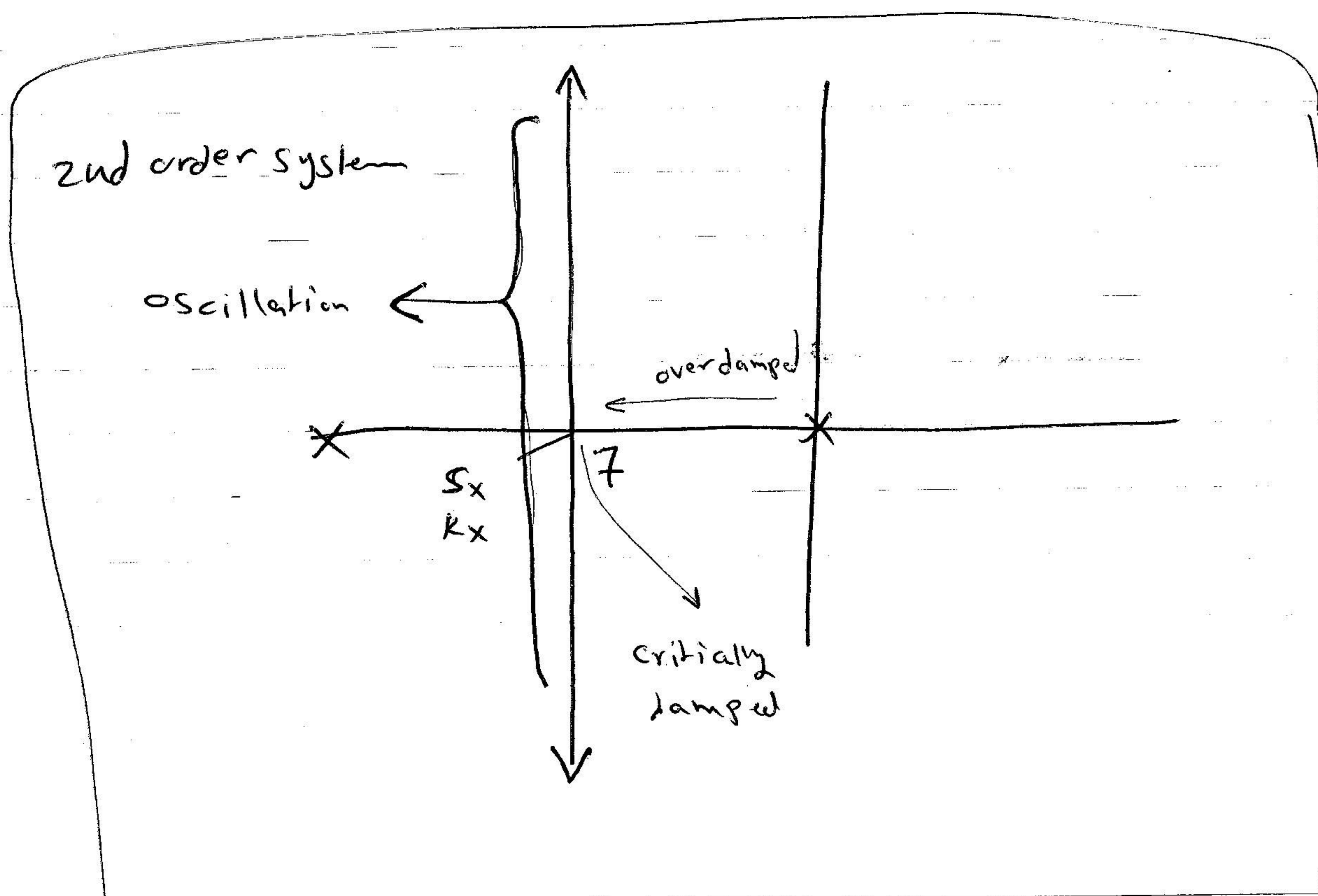
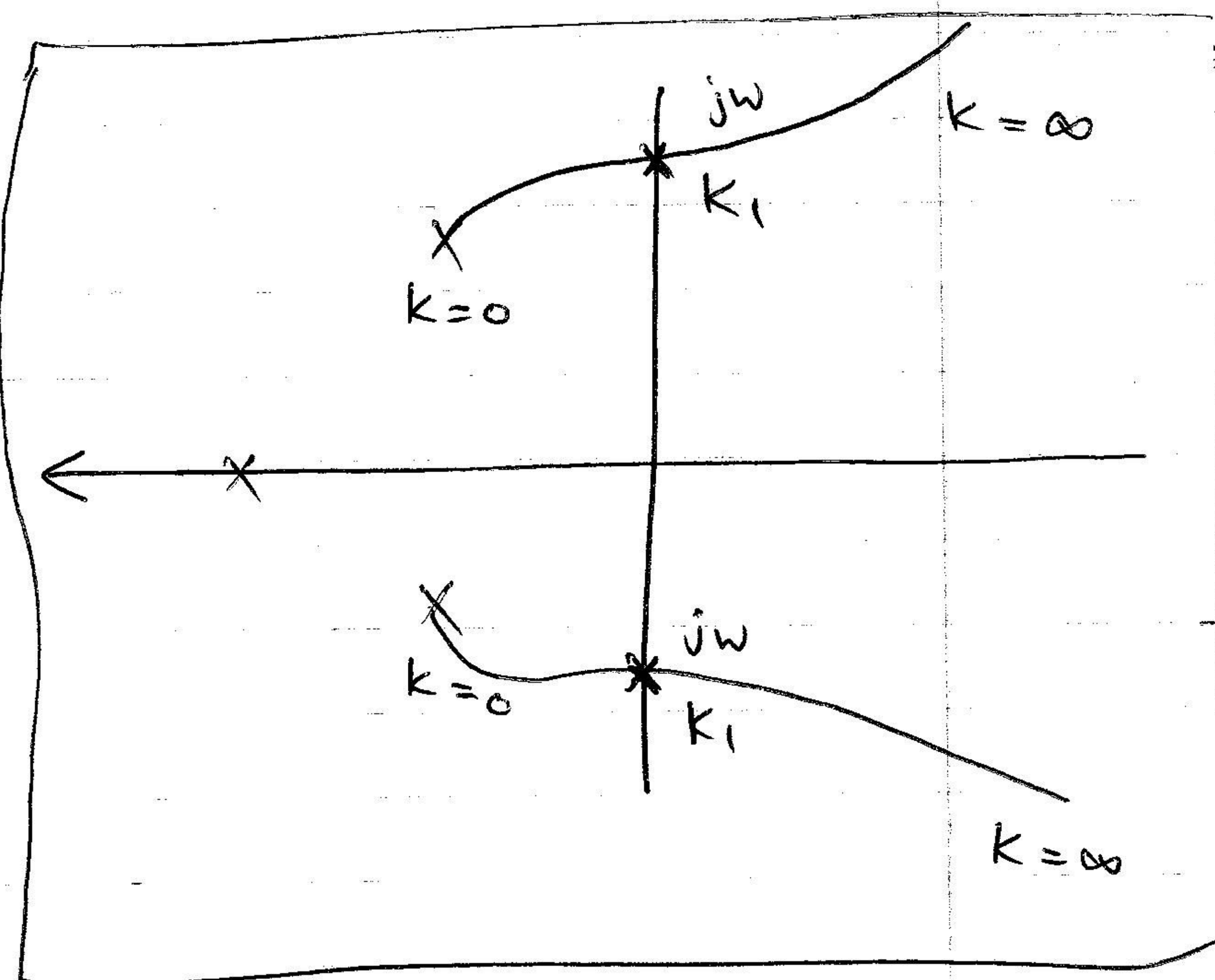
زاوية الوصول
for zeros

STEP 11 PLOT (take in consideration all the previous steps and plot the system).

STEP 12

Determine the parameter value k_x & specific root s_x

$$k = \frac{\prod_{j=1}^n (s + p_j)}{\prod_{i=1}^m (s + z_i)}$$



Example plot the root locus for the ch. equ., as K varies from zero to infinity

$$G(s) = 1 + \frac{K}{s^4 + 12s^3 + 64s^2 + 128s}$$

STEP 1 DONE

STEP 2 DONE

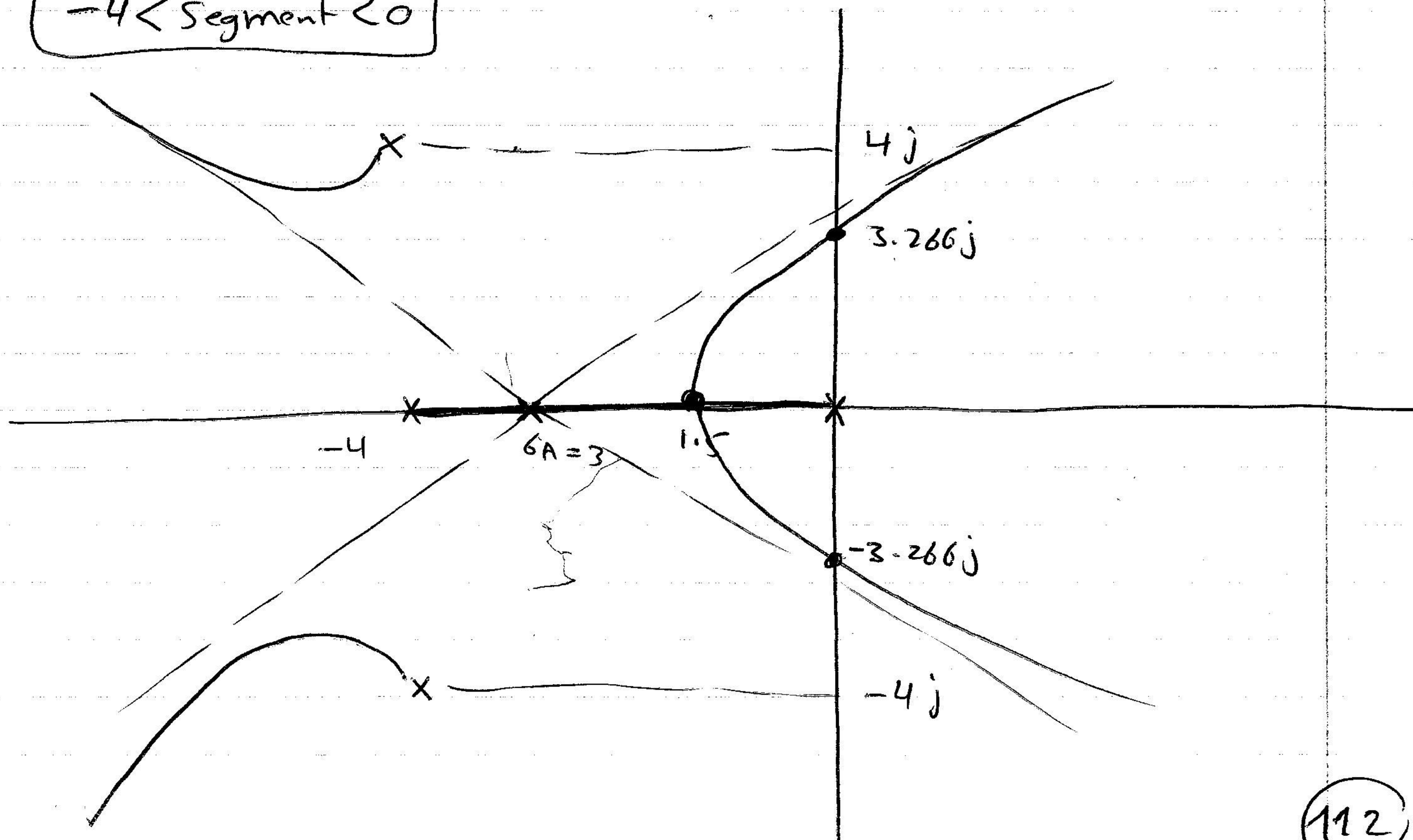
STEP 3 ~~NO ZEROS~~

~~Poles:~~ $1 + \frac{K}{s(s+4)(s+4+4j)(s+4-4j)}$

STEP 4 Zeros : No Zeros

Poles : $s = \underline{0}, \underline{-4}, \underline{-4-4j}, \underline{-4+4j}$

$-4 < \text{Segment} < 0$



STEP 5 Number of separate loci = $N_p = 4$

STEP 6 σ To be taken in consideration.

STEP 7 $\phi_A = \frac{\sum \text{poles} - \sum \text{zeros}}{N_p - N_z} = \frac{-4 + -4 + -4 + 0}{4} = -3$
 $(q = 0, 1, 2, 3)$

$\phi_A = \frac{2q+1}{4-0}$

$\phi = 45^\circ, 135^\circ, 225^\circ, 315^\circ$

$q = 0 \quad 1 \quad 2 \quad 3$

STEP 8 ch. equ. $q(s) = s^4 + 12s^3 + 64s^2 + 128s + k = 0$

s^4	1	64	k
s^3	12	128	0
$\rightarrow s^2$	53.33	k	0
s^1	C_1	0	
1	k		

Auxiliary equation

C_1 must be zero $\Rightarrow k = 568.89$

استقرار النظام
 $0 \rightarrow k$

Auxiliary Equation :-

$53.33 s^2 + 568.89 = 0 \Rightarrow s_{1,2} = \pm j 3.266$

STEP 9

k	0	75	85	80	68	51	0
s	0	-1	-1.5	-2	-2.5	-3	-4

STEP 10 Angle of Departure $\Phi = 225^\circ$

STEP 11 Plot (go back to the plot page 112)

STEP 12 ~~Plot~~

Stable for $0 < K < 568.89$

اے کی دنیا امتحان ہو سکتی

بالوفیق للجميع



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